



Some optical design techniques
and general methods

From my 56 years in Optical design

Dave Shafer
June 2022

#1

Even very simple designs often have more than one possible version, so investigate to see which is the best one.

Example – there are always two different bending shapes of a single lens that have the same amount of 3rd order spherical aberration, but they differ in the 5th order. See which is the best choice in the design it is part of.

Another example

A high performance two element catadioptric optical design

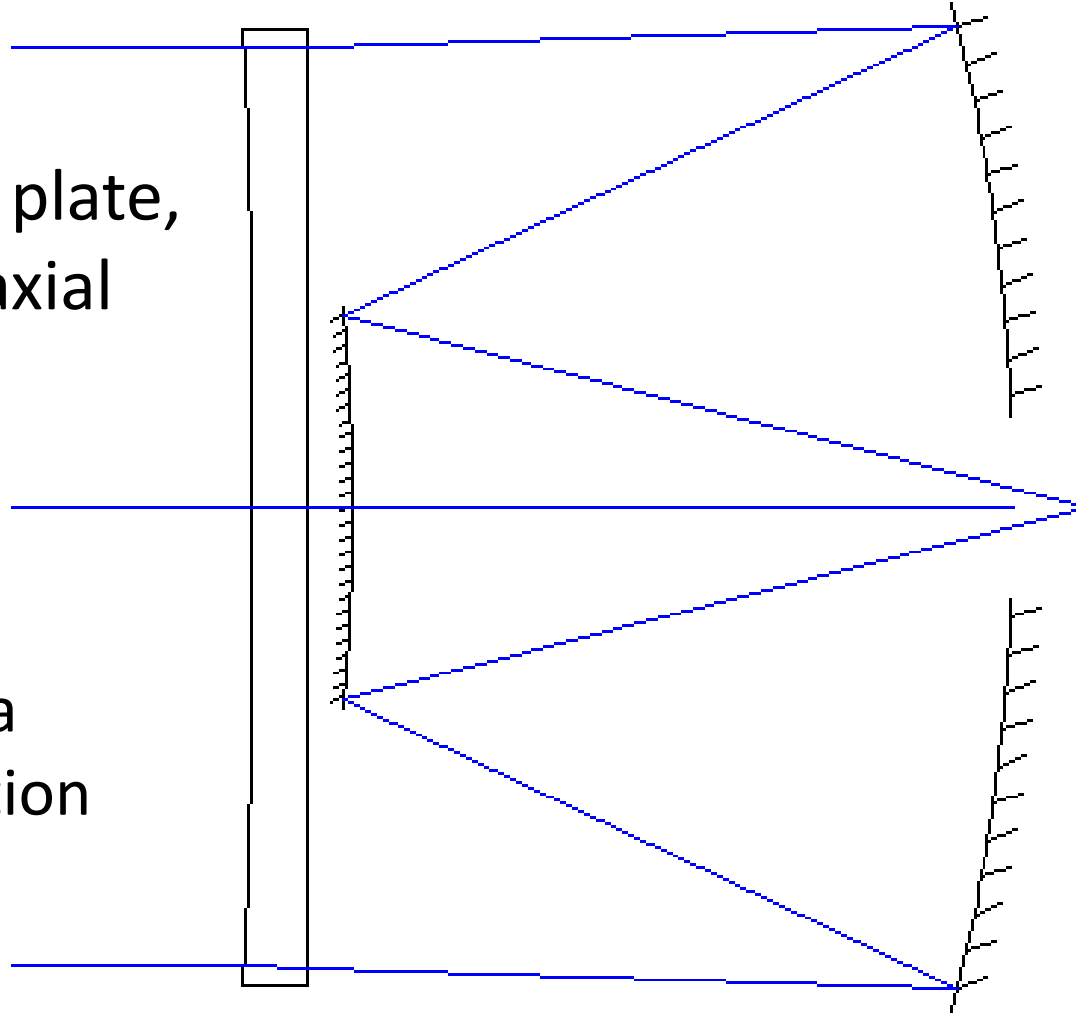
No name
FOCAL LENGTH = 200 NA = 0.25

UNITS: MM
DES: OSLO

22.2

Aspheric plate,
zero paraxial
power

17% area
obscuration



Aspheric
primary and
secondary
mirrors

Typical
Schmidt-
Cassegrain
design.

Three aspherics
and equal mirror
radii gives
correction for
spherical
aberration, coma,
astigmatism
and Petzval

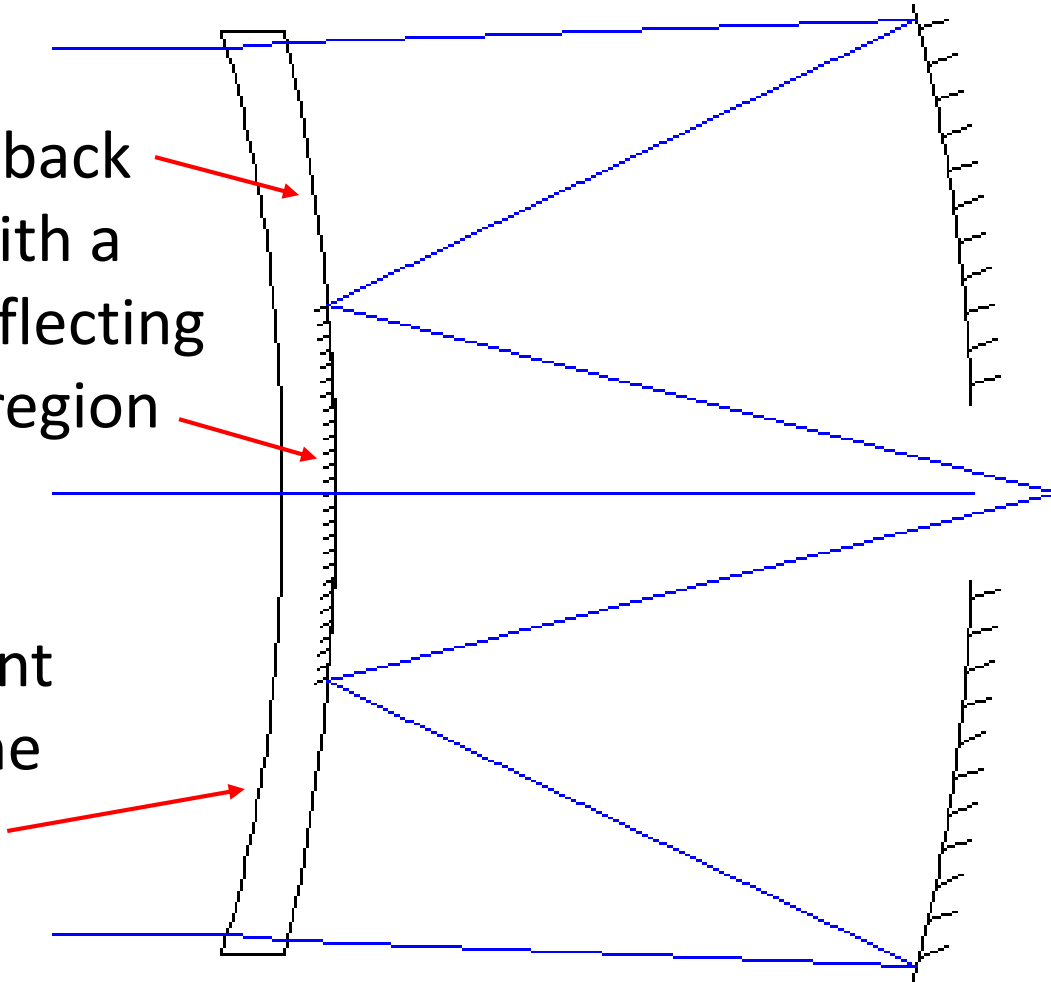
No name
FOCAL LENGTH = 200 NA = 0.25

UNITS: MM
DES: OSLO

22.2

Spherical back
surface with a
central reflecting
aspheric region

Aspheric front
surface of the
zero power
element



Same
aspherics,
same
aberration
correction.

Secondary
mirror has
same radius as
back of front
element, but
not the same
surface.

**Curve the
front zero
power
element**

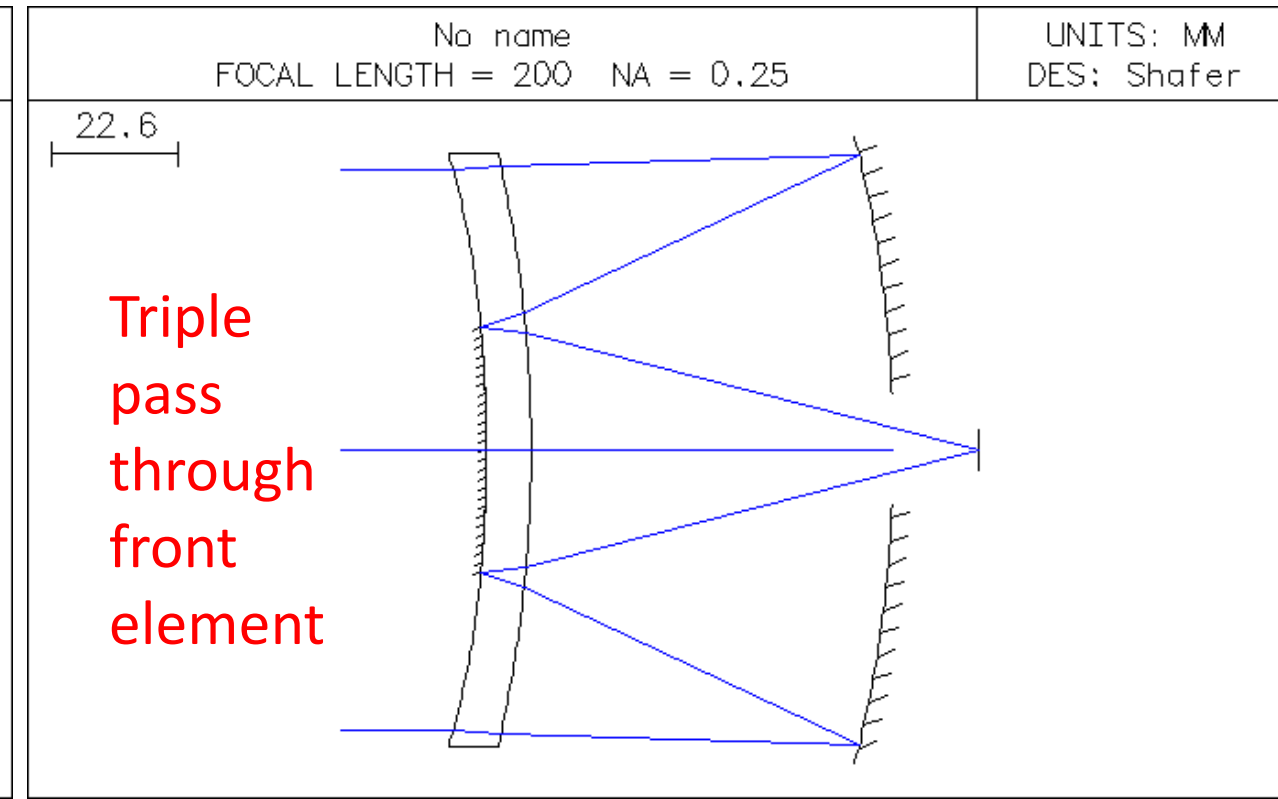
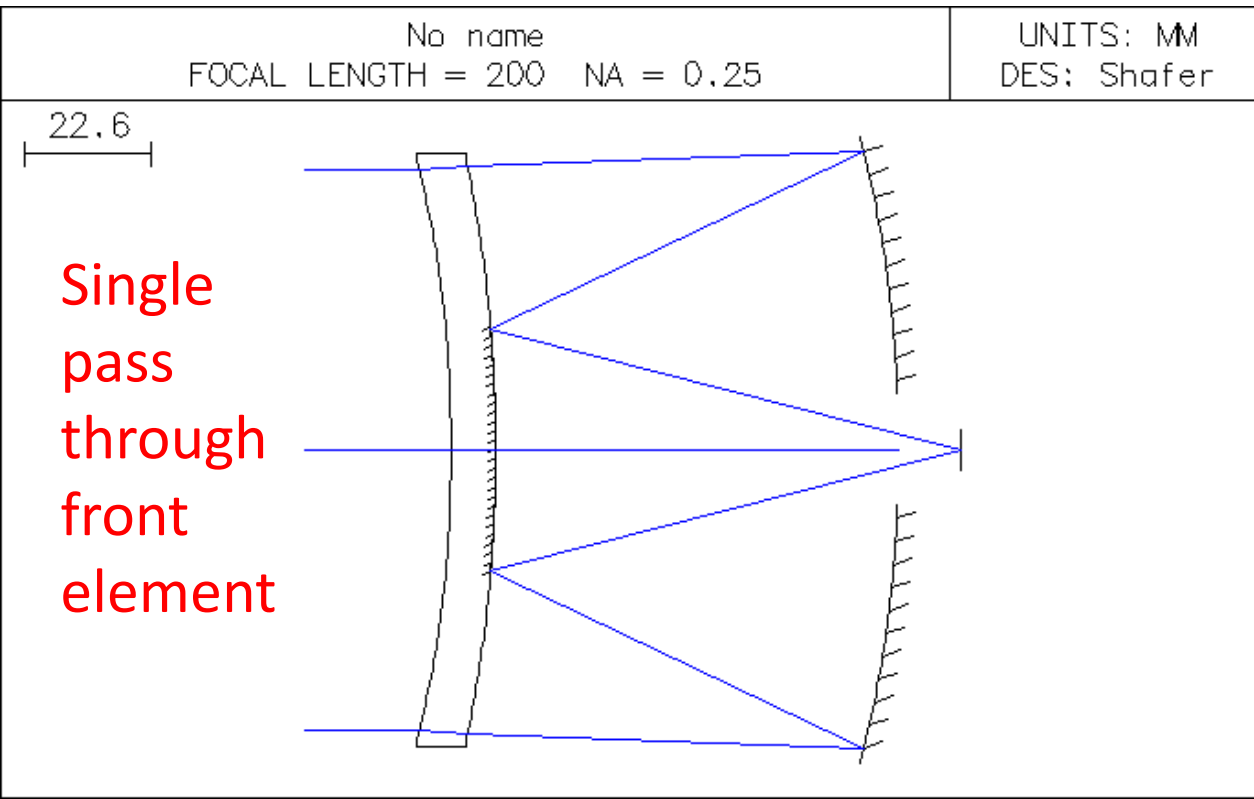
There are 4 possibilities for a design with three aspherics

Case #1 – front surface of front lens = aspheric, back surface is spherical with aspheric middle portion

Case #2 – front surface of front lens is spherical, back surface is aspheric with a different aspheric middle portion

Case #3 – front surface of front lens is spherical with a central reflecting aspheric region. Back surface is aspheric

Case #4 – front surface of front lens is aspheric with a different aspheric central reflecting area. Back surface is spherical

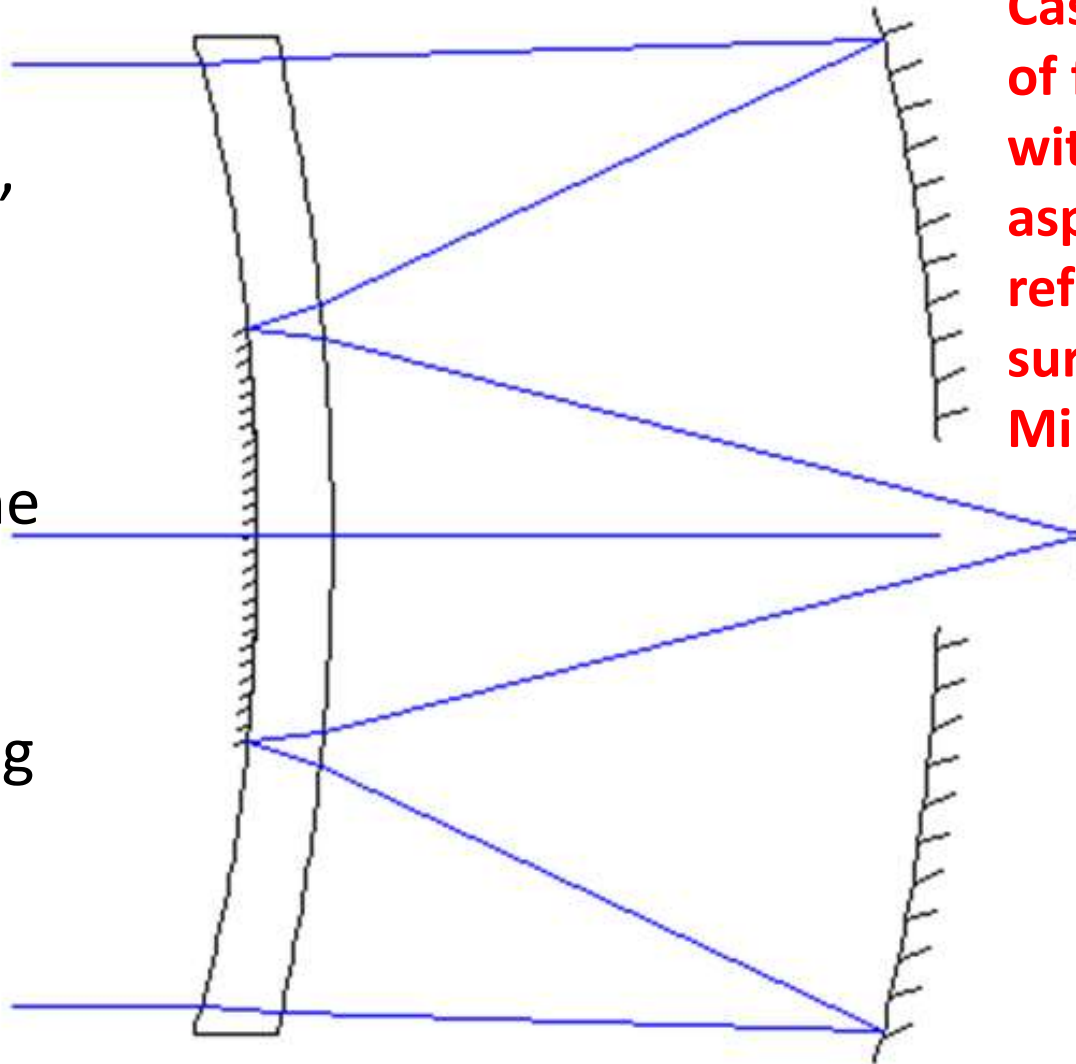


No name
FOCAL LENGTH = 200 NA = 0.25

UNITS: MM
DES: Shafer

22.6

When spherical aberration, coma, astigmatism, and Petzval are corrected in the Case #4 design the aspheric front surface and the aspheric reflecting middle area have very similar aspherics



Case #4 – front surface of front lens is aspheric with a different aspheric central reflecting area. Back surface is spherical. Mirror is aspheric

Front lens is zero power

No name
FOCAL LENGTH = 200 NA = 0.25

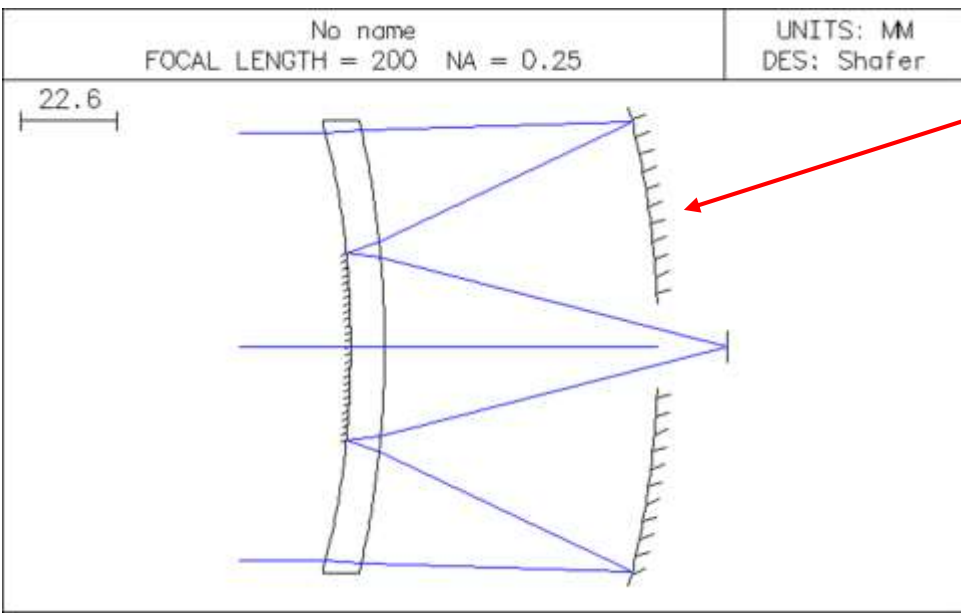
UNITS: MM
DES: Shafer

22.6
BK7 glass

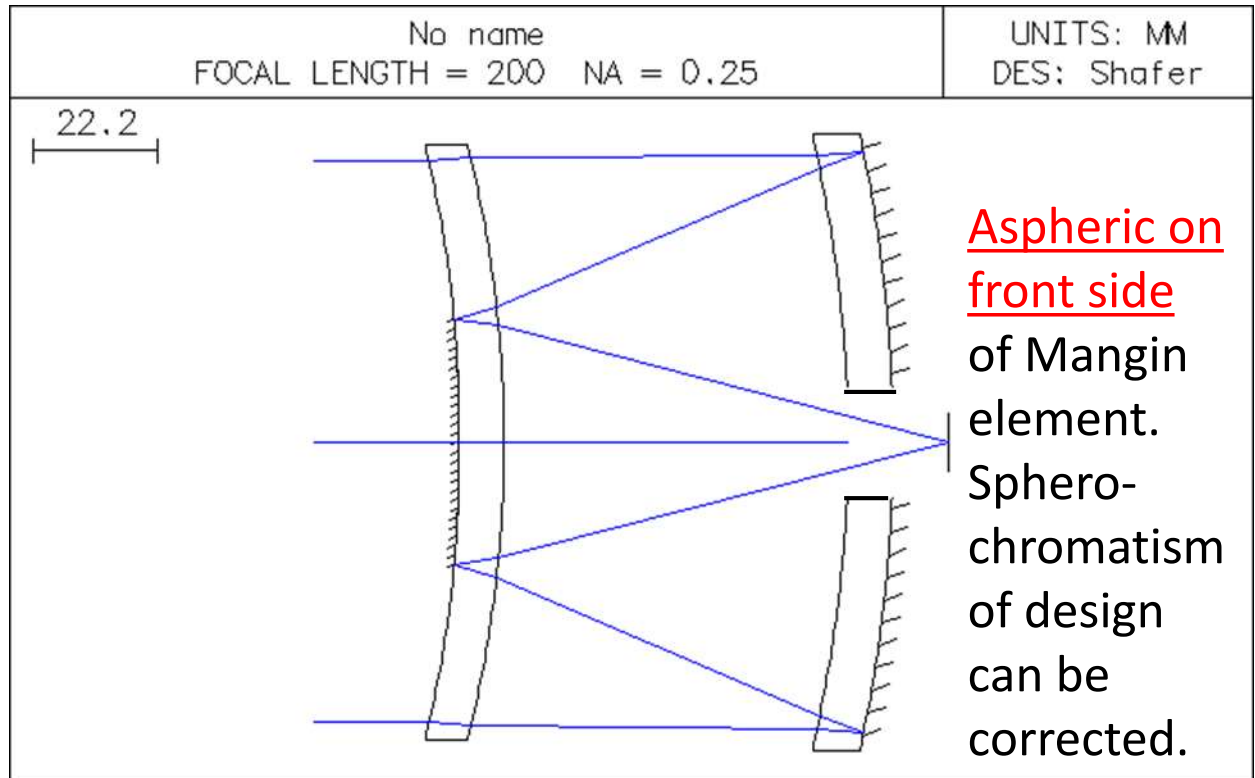
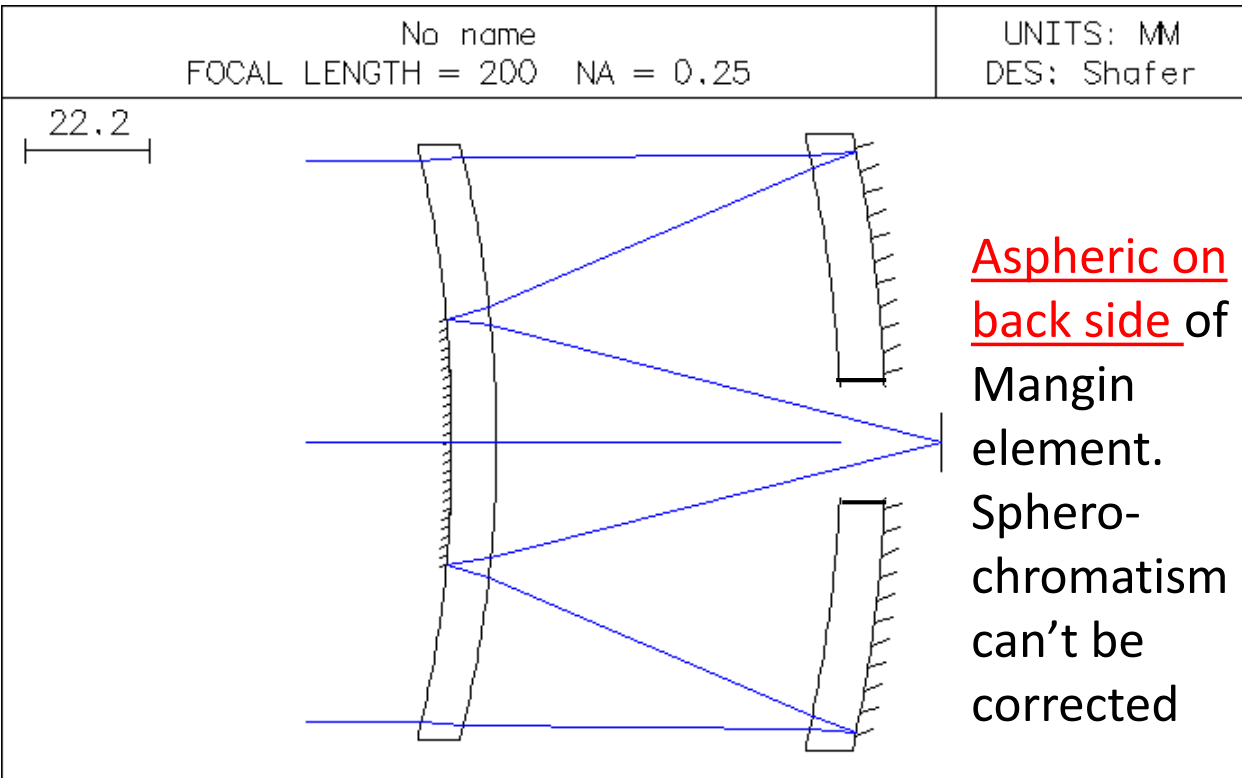
Diffraction-limited
monochromatically
over the field but bad
chromatic variation of
spherical aberration.

Result is 200 mm
focal length f/2.0
with a 3 degree
diameter flat field
and **paraxial axial
color correction.**

By a small change
in the first order
parameters the
front surface
aspheric and the
middle region
aspheric on the
front surface can
be made the same,
as well as having
the exact same
curvature. **The
result is a well
corrected design
with only two
separate aspherics**



The aspheric mirror can be replaced with a Mangin mirror element to get an extra design variable and that can be used to correct the design's chromatic variation of spherical aberration. The Mangin element has essentially the same radius on both sides as does the front lens so axial color is zero. The aspheric might go on the front or the back of the element.



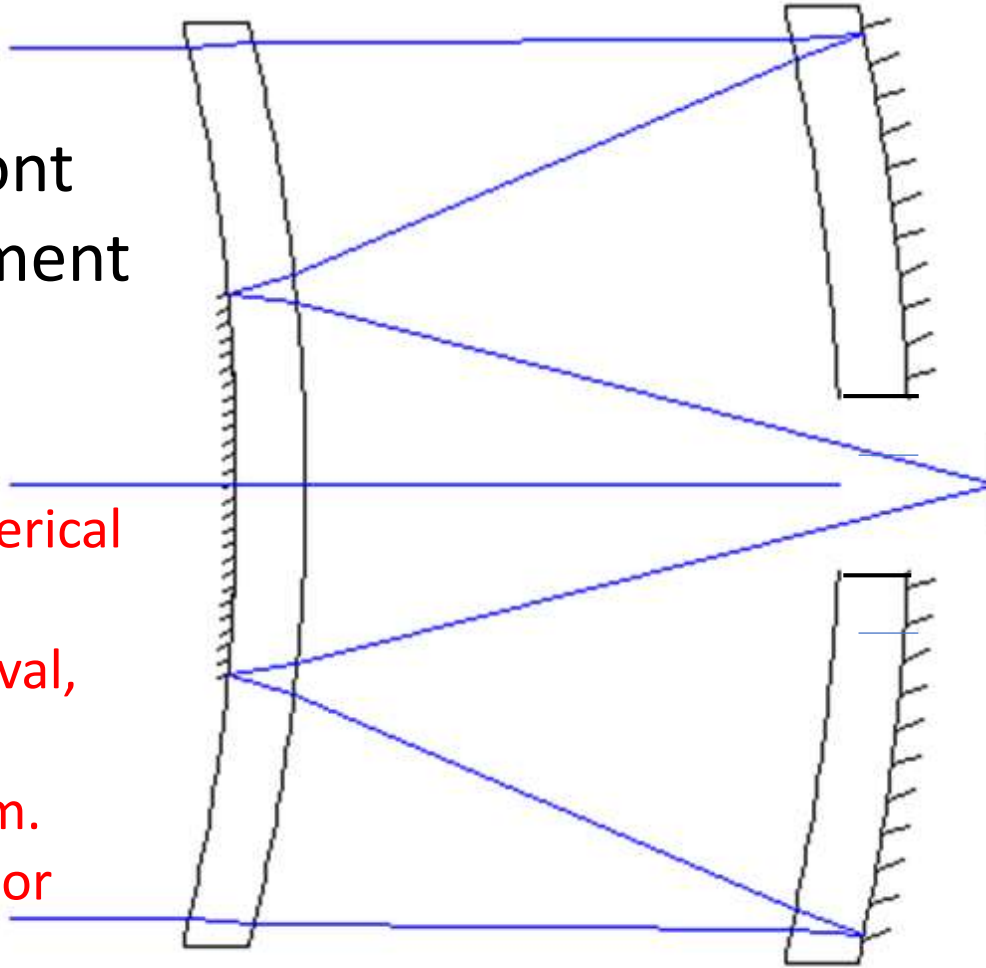
No name
FOCAL LENGTH = 200 NA = 0.25

UNITS: MM
DES: Shafer

22.2

Aspheric front
side of element

Corrected for spherical
aberration, coma,
astigmatism, Petzval,
axial color and
spherochromatism.
But not lateral color
(a small amount)



Aspheric
front side of
Mangin
element

f/2.0 design with 3
degree field
diameter and
diffraction-limited
monochromatically
over field. Axial
color and sphero-
chromatism is
corrected but there
is still **lateral color**.
How to correct
without adding any
elements?

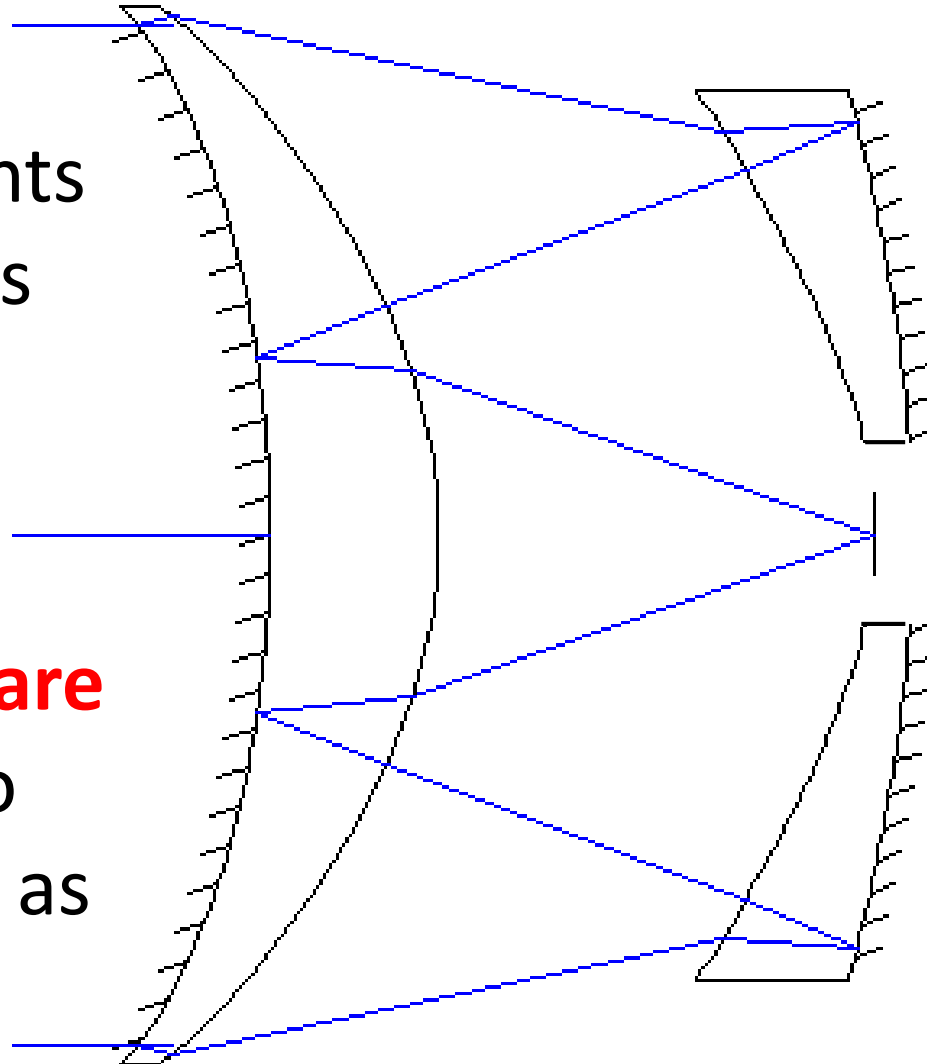
No name
FOCAL LENGTH = 100 NA = 0.3333

UNITS: MM
DES: Shafer

14.5

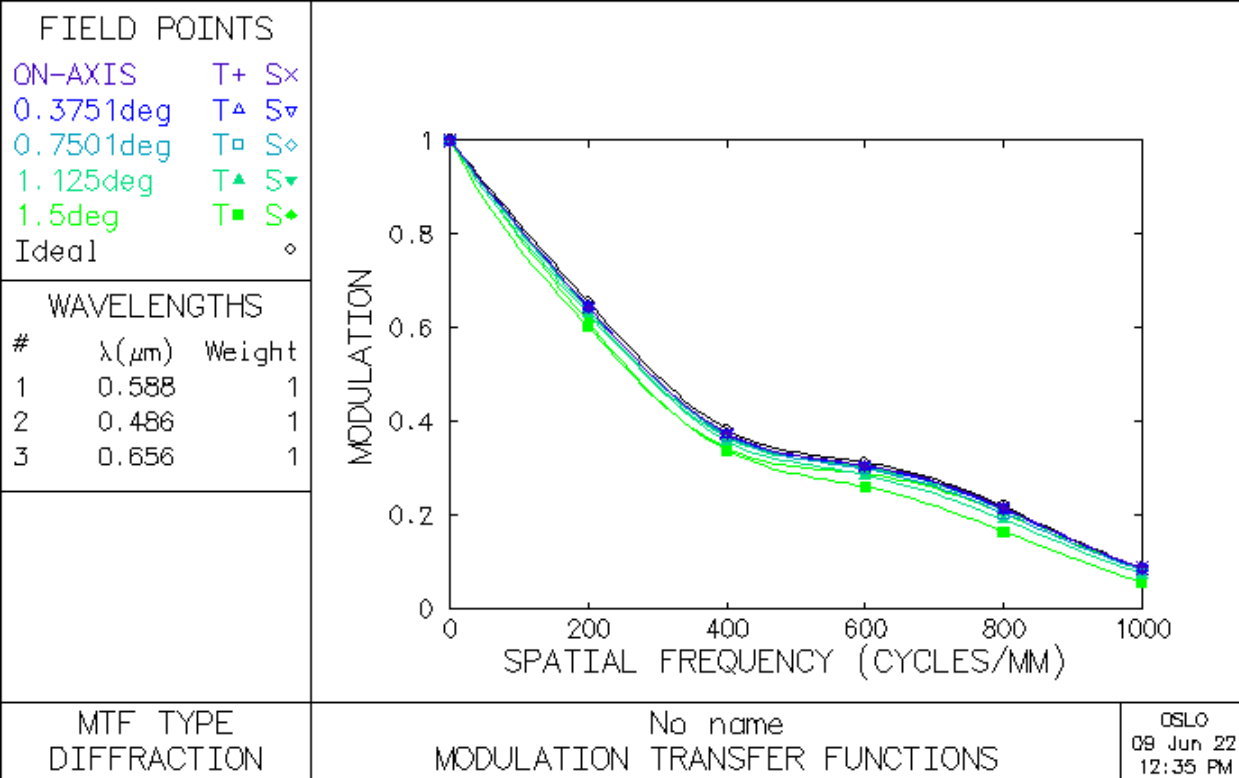
Both elements
are BK7 glass

**All 4 surfaces are
aspheric** = two
new aspherics as
variables



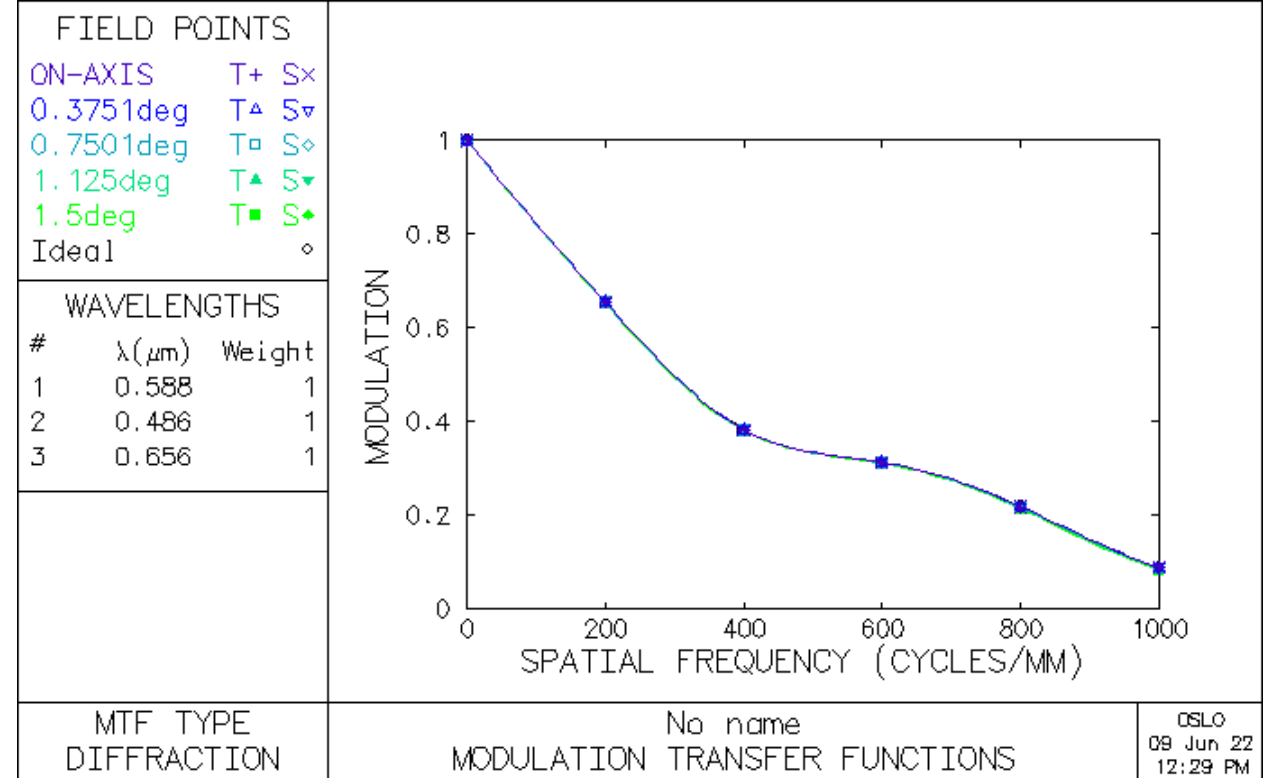
**With extra
aspherics we get
this new solution**

New design has
faster f/1.5 speed
plus **axial and
lateral color and
spherochromatism**
correction



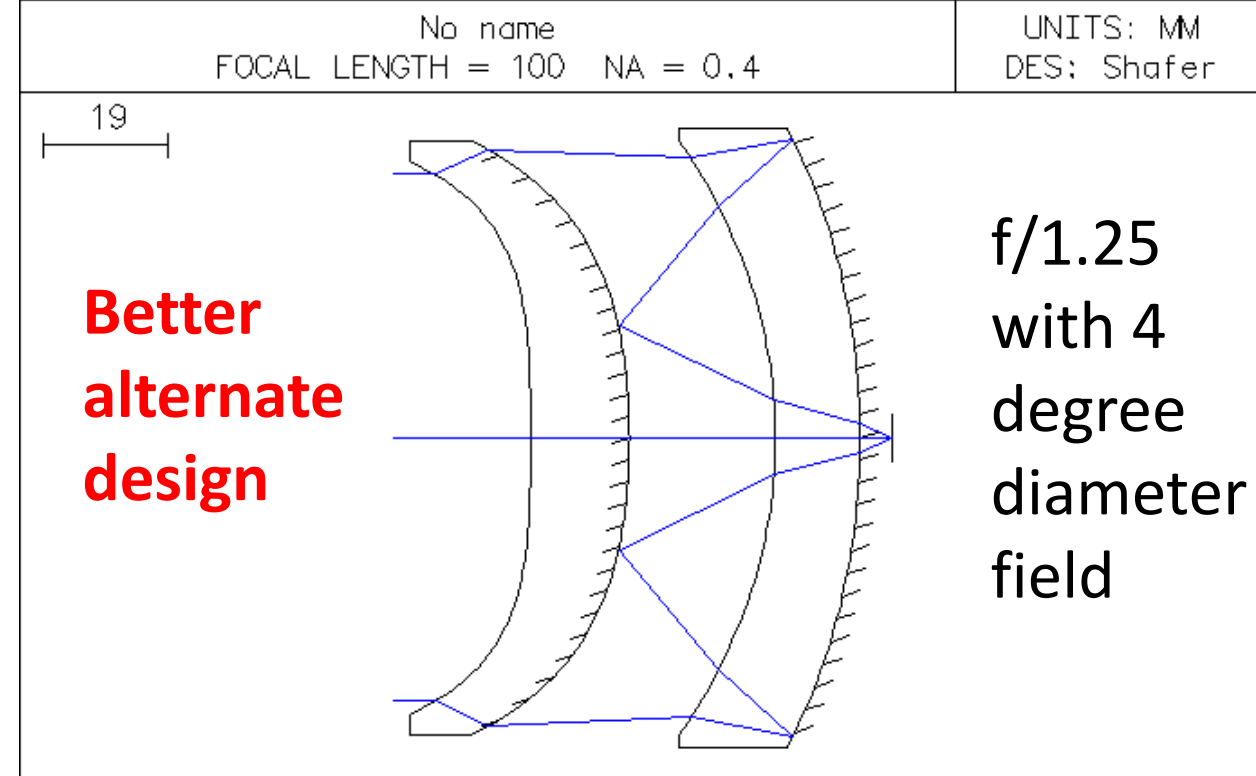
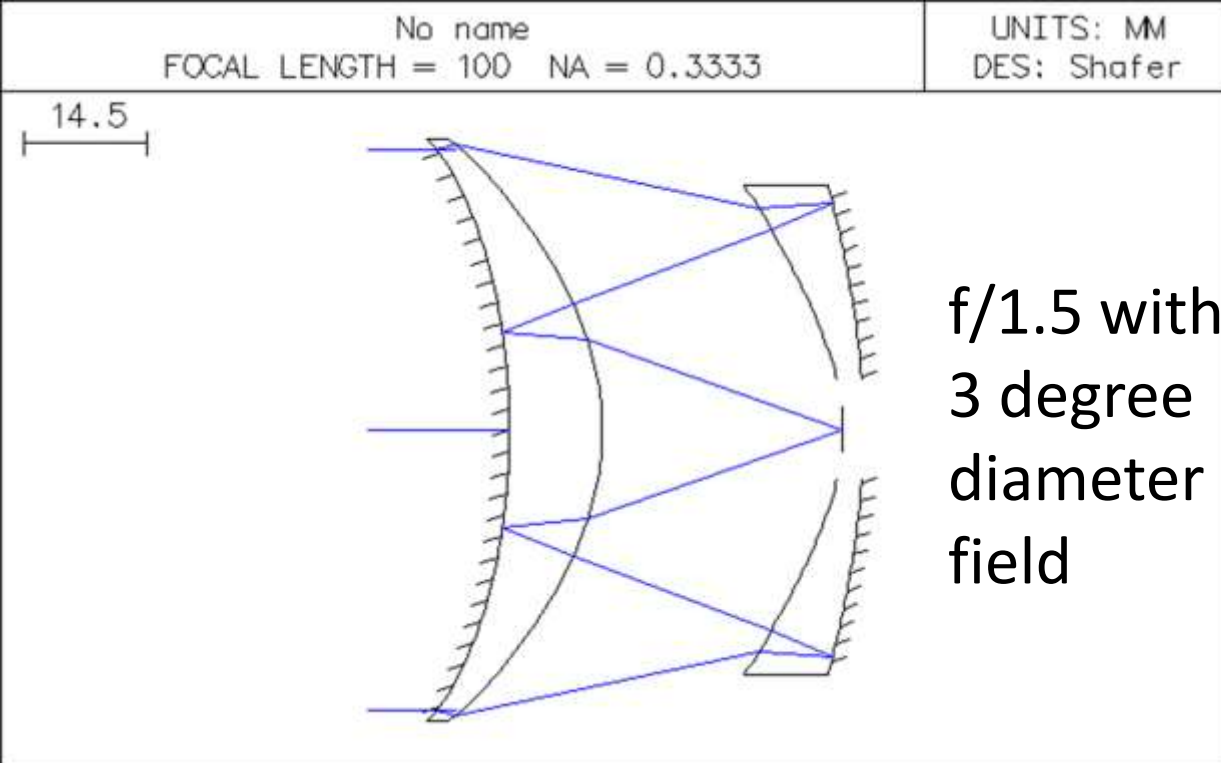
Actual 100 mm focal length f/1.5
design with 3 degree diameter field
and 35% obscuration

35% diameter obscuration



Perfect system with
35% obscuration

**So now we are finished, right?
Wrong! There is a better
alternate solution that was found
after this one was found.**

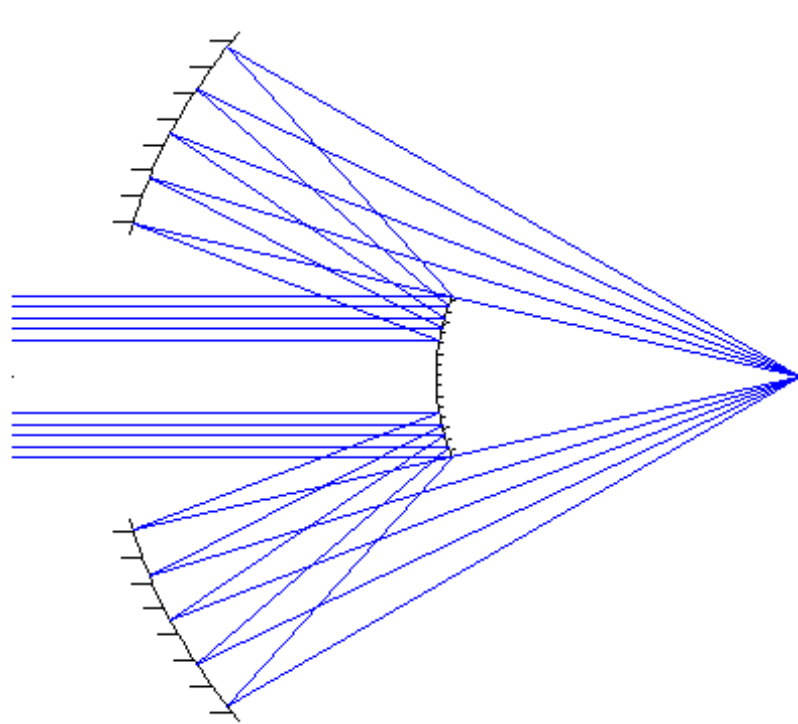


Both designs are just two BK7 elements with 4 aspherics and good color correction but the one on the right is much better. They both evolved from different starting points with the one on the left having a triple pass through the front element while the one on the right has a single pass through that front element.

This shows how even a very simple design can have several good solutions and one will be the best one. But you have to go looking for it.

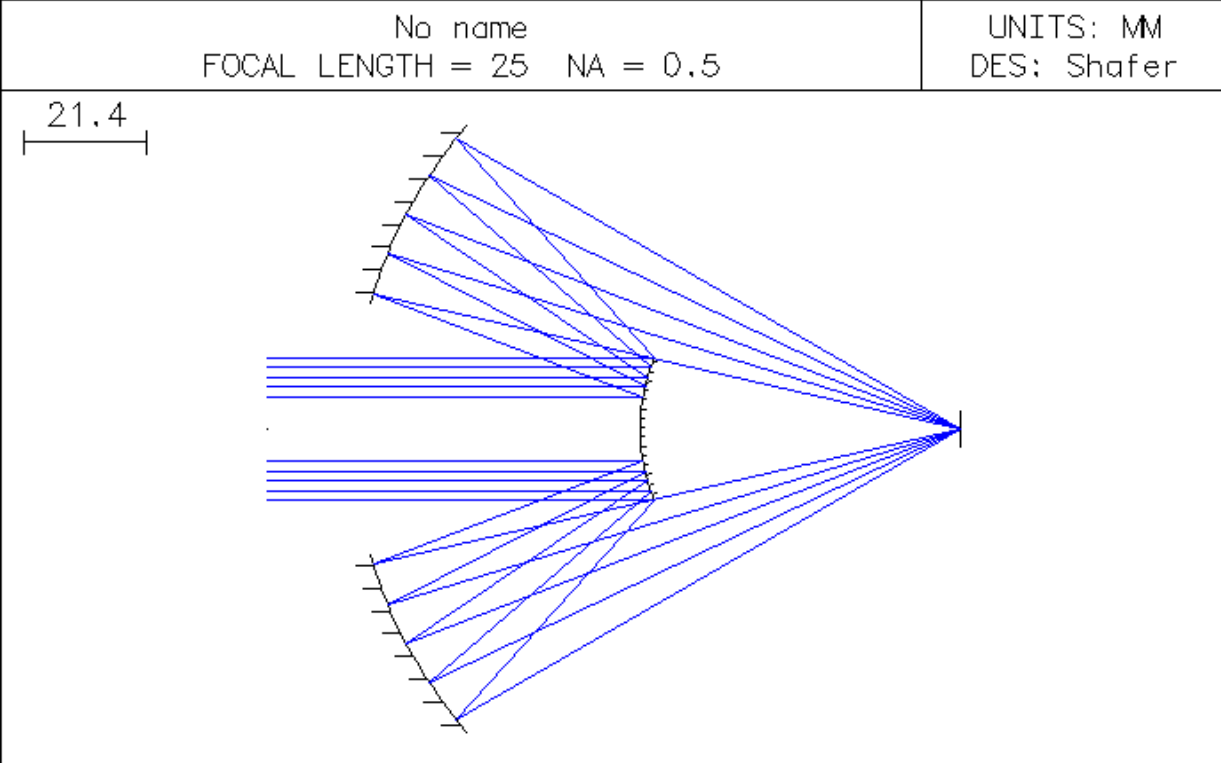
No name
FOCAL LENGTH = 25 NA = 0.5

UNITS: MM
DES: Shafer

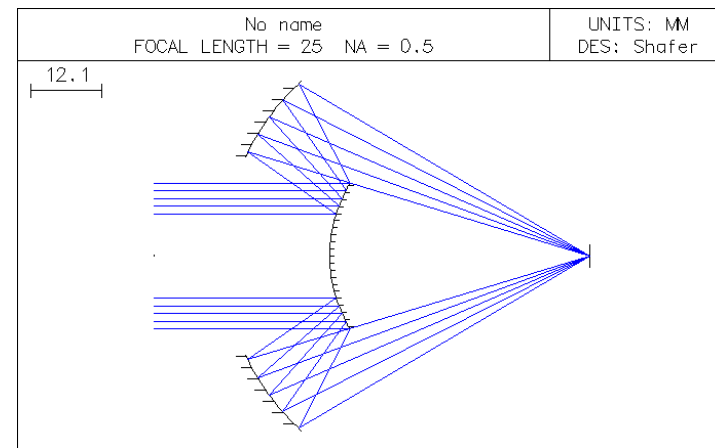


Another example

Suppose you want to focus a collimated beam of light and want the design to have a broad spectral band and be simple and inexpensive. You could use the Schwarzschild design of two concentric spherical mirrors, which is well-corrected for spherical aberration, and also coma and astigmatism. But the concave mirror is large and the diameter obscuration is 45%.



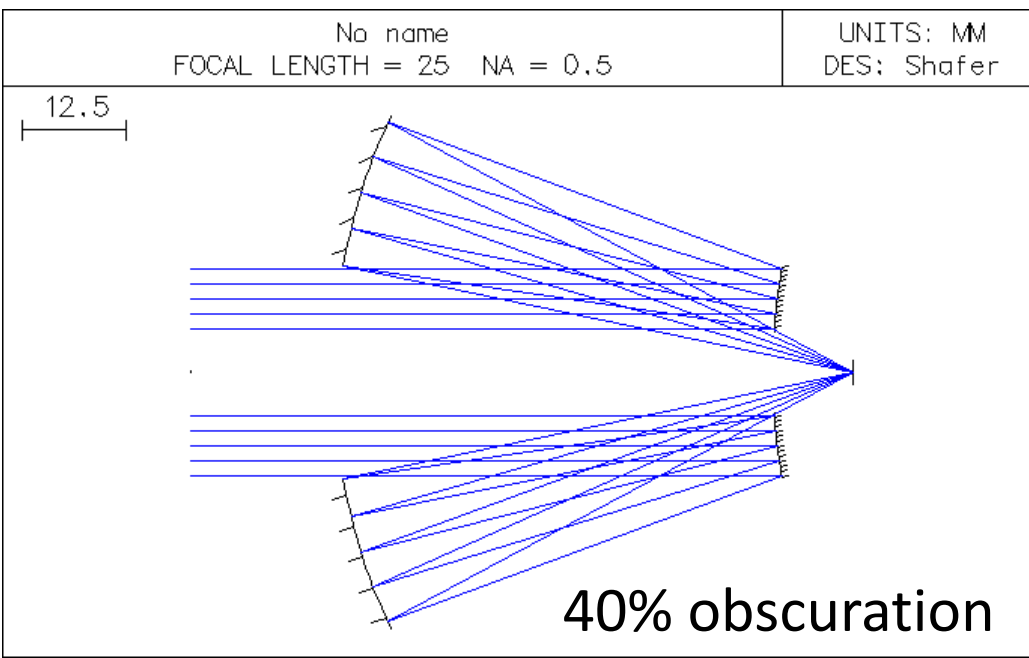
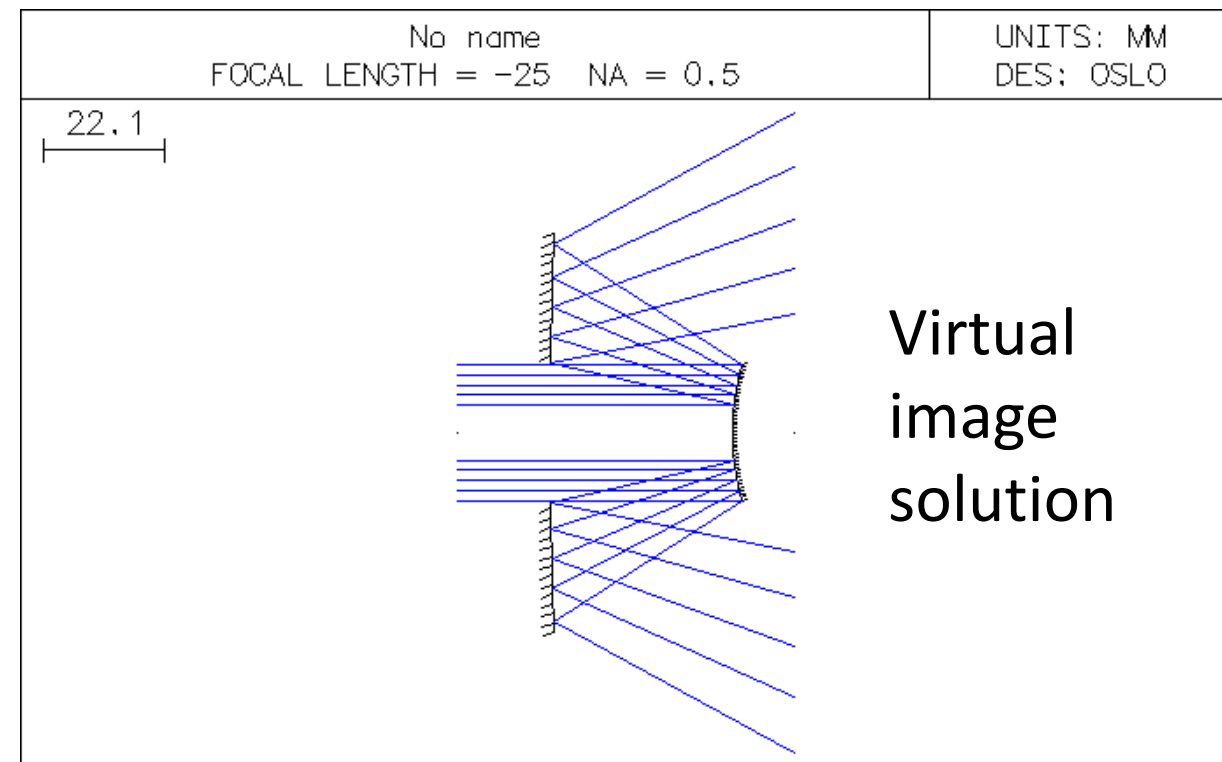
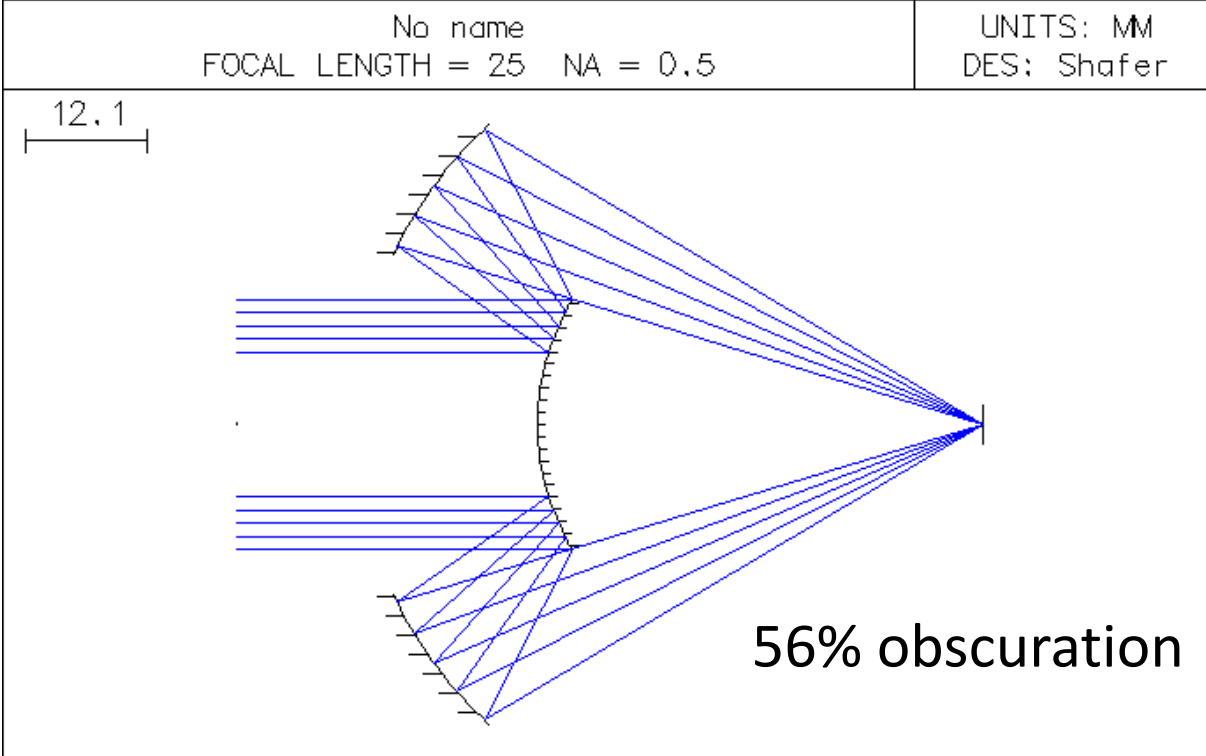
Large mirror is 4.24X entering beam diameter. 45% obscuration.



Same scale for 25 mm f.l and f/1.0

Large mirror is 2.5X entering beam diameter. 56% obscuration. Coma not corrected.

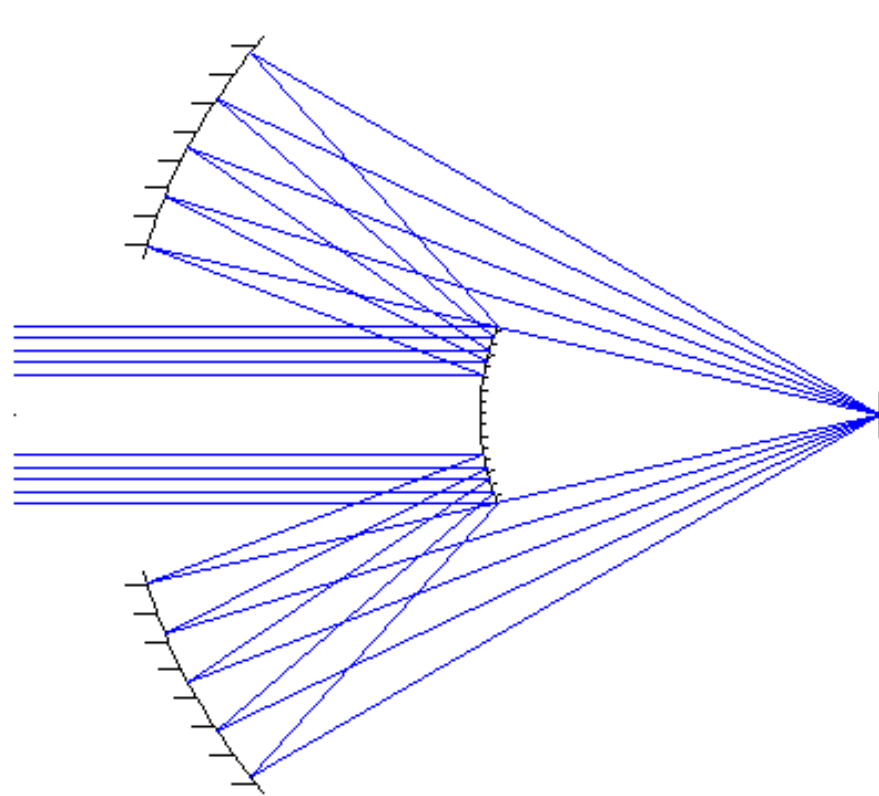
Concave mirror is moved closer to convex mirror to give smaller size. Then concave radius is solved to correct for spherical aberration. Result has larger obscuration. There is only one variable – the concave mirror radius – and only one aberration – spherical aberration – so there is only one solution right? Wrong! There are 3!!



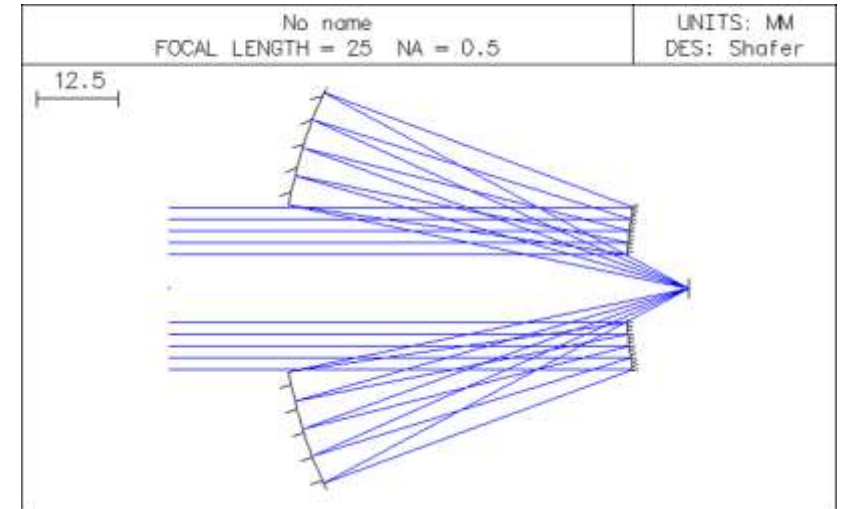
Three different solutions for the concave mirror that correct for spherical aberration. This is a 1 X 1 optimization matrix and yet there are these multiple solutions. But only the Schwarzschild design with a much bigger concave mirror also has coma correction.

No name
FOCAL LENGTH = 25 NA = 0.5

UNITS: MM
DES: Shafer



Most compact
solution of the 3
solutions with 2.5X
concave mirror size



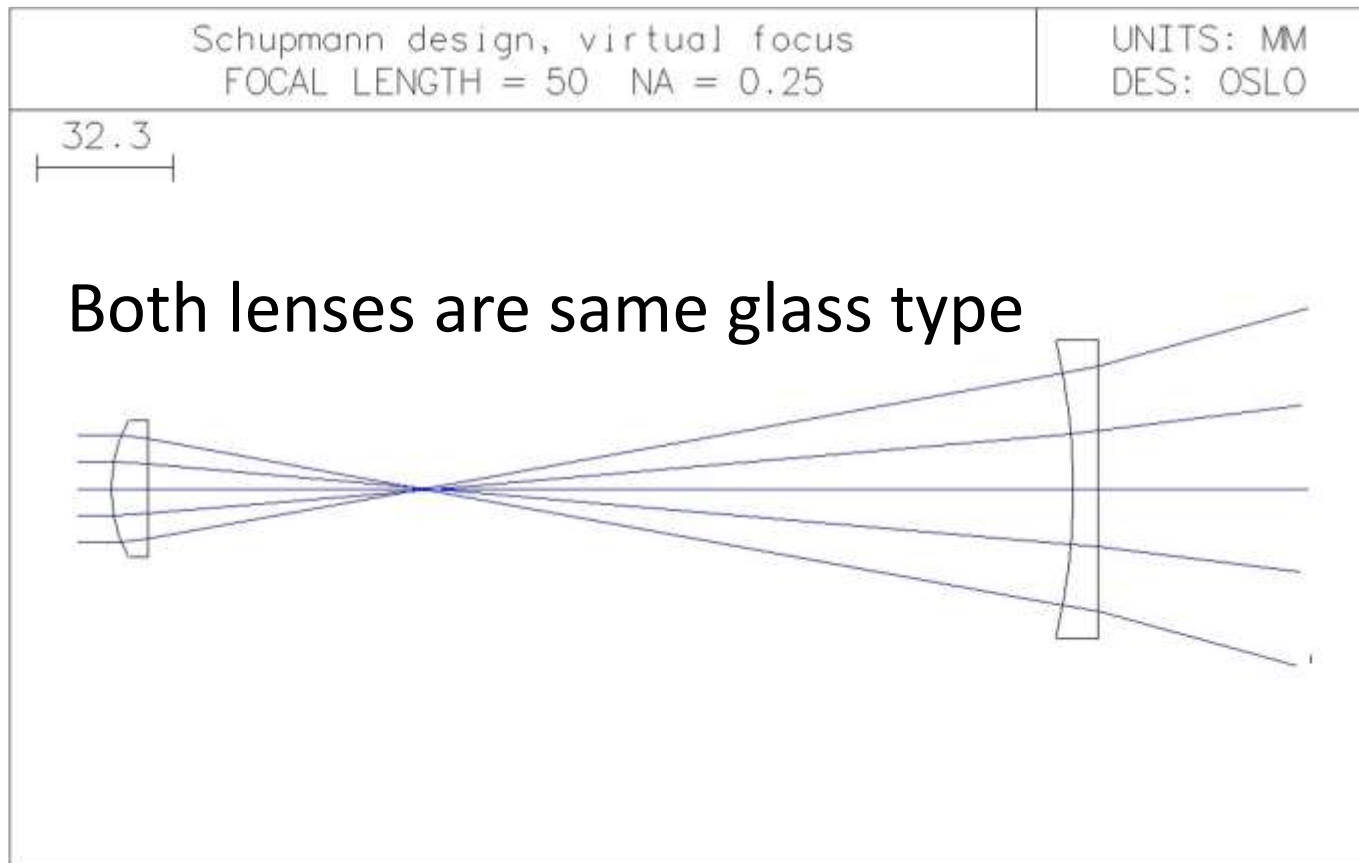
Schwartzschild concentric
design with concave mirror
4.24X larger than entering beam

Same focal length

#2

Simple systems with useful properties can be combined to make new types of designs.

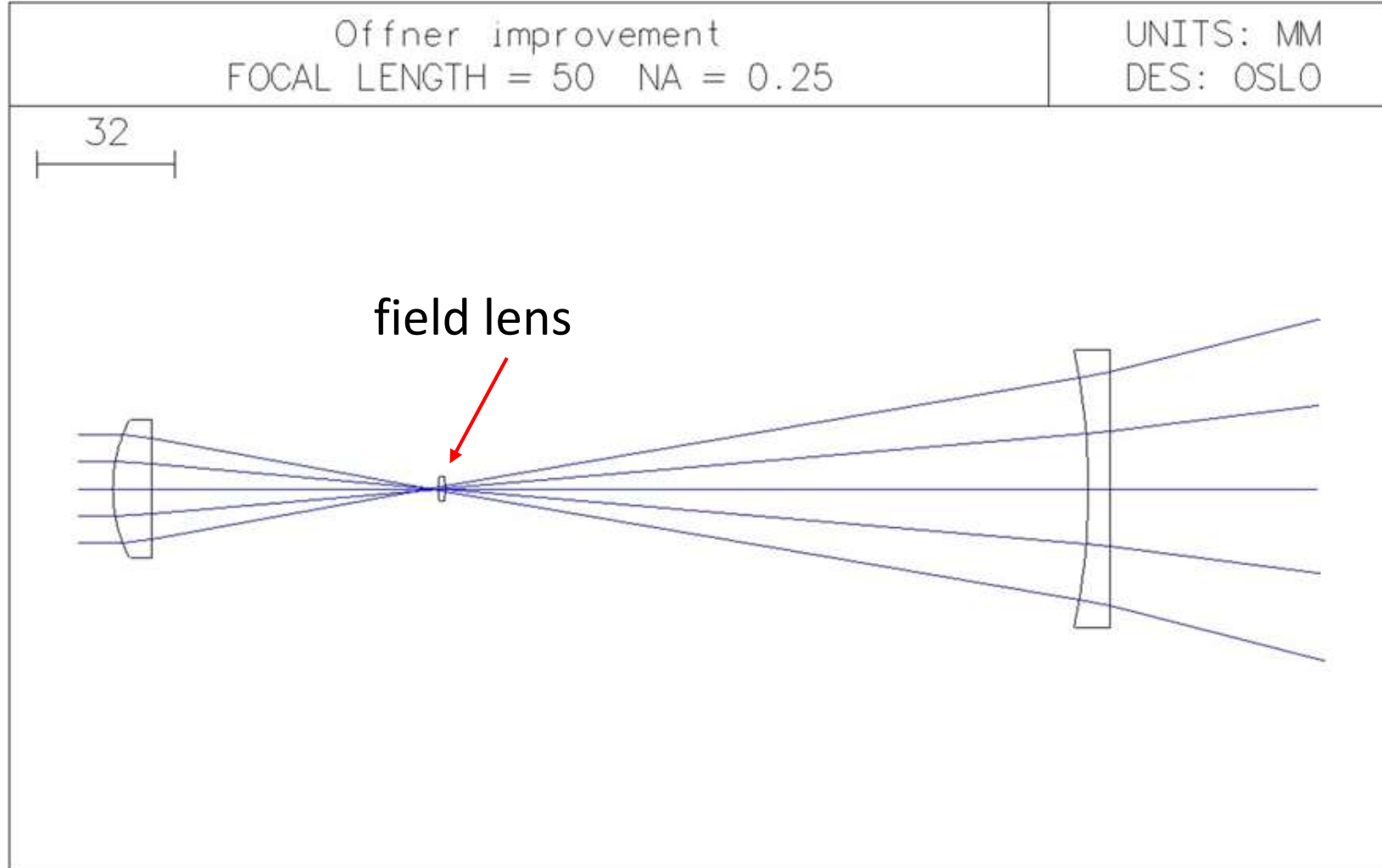
Example – the CMO design



This simple design is not useful by itself, since it does not form a real image, but a virtual one. But it is a good building block in more complex designs.

Schupmann design with virtual focus

Axial color is linear with lens power, quadratic with beam diameter, so axial color here cancels between the lenses, one small with strong power and one large with weak power.

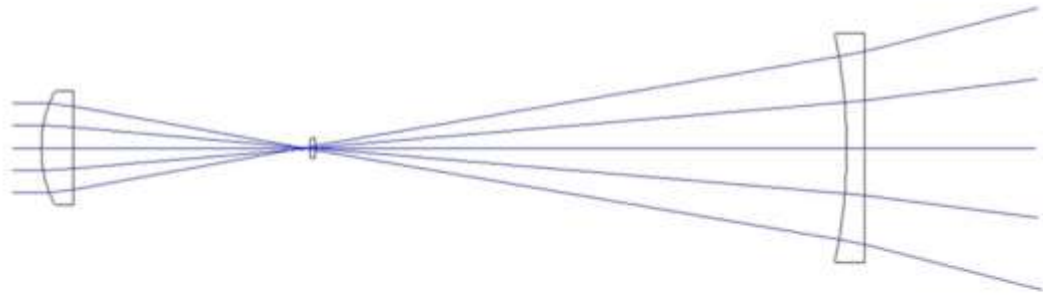


Offner improvement – a field lens at the intermediate focus.
The field lens images the other two lenses onto each other.
That corrects the design for lateral color. Why?

Offner improvement
FOCAL LENGTH = 50 NA = 0.25

UNITS: MM
DES: OSLO

32



Virtual image design

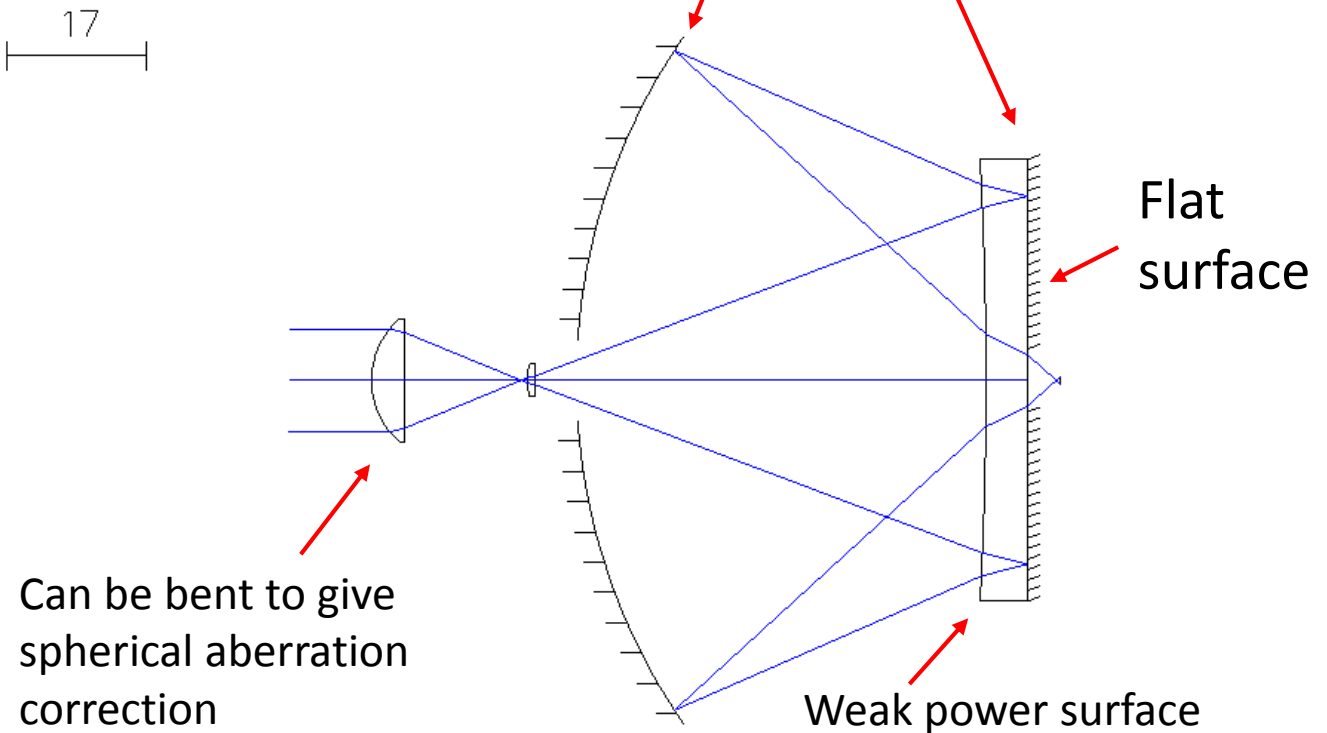
Concave mirror reflection speeds up real image $f\#$ by about 2X to give a faster speed design, yet adds no color. New design has small obscuration near final image due to hole in flat reflecting surface.

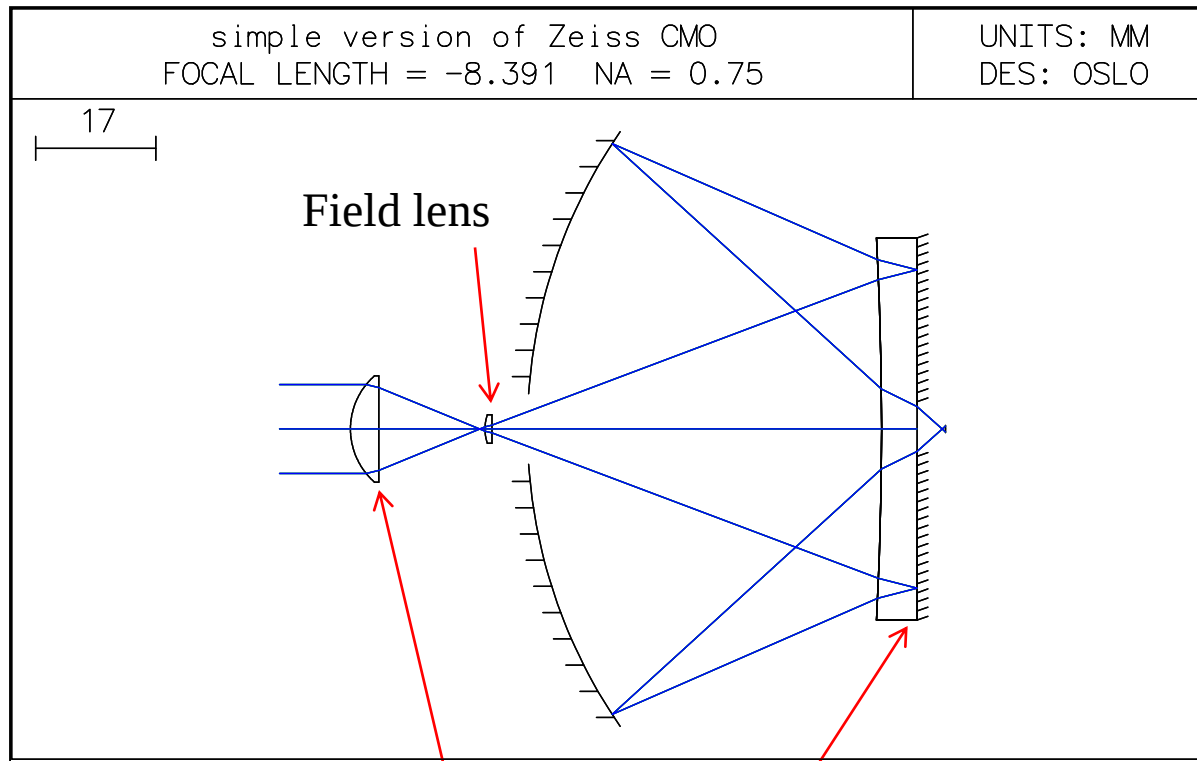
Virtual image from Schupmann design is made into a **real** image by adding two mirror surface reflections here.

simple version of Zeiss CMO
FOCAL LENGTH = -8.391 NA = 0.75

UNITS: MM
DES: OSLO

17





Low-order theory of design

- 1) Put stop on first lens, then choose power of field lens to image it onto the lens/mirror element. Stop is then effectively at both places.
- 2) Then neither of those elements has lateral color. Power of lens/mirror element corrects axial color.
- 3) Field lens imaging and only one glass type corrects for secondary axial color too (Offner theory).
- 4) Then can put the stop anywhere.

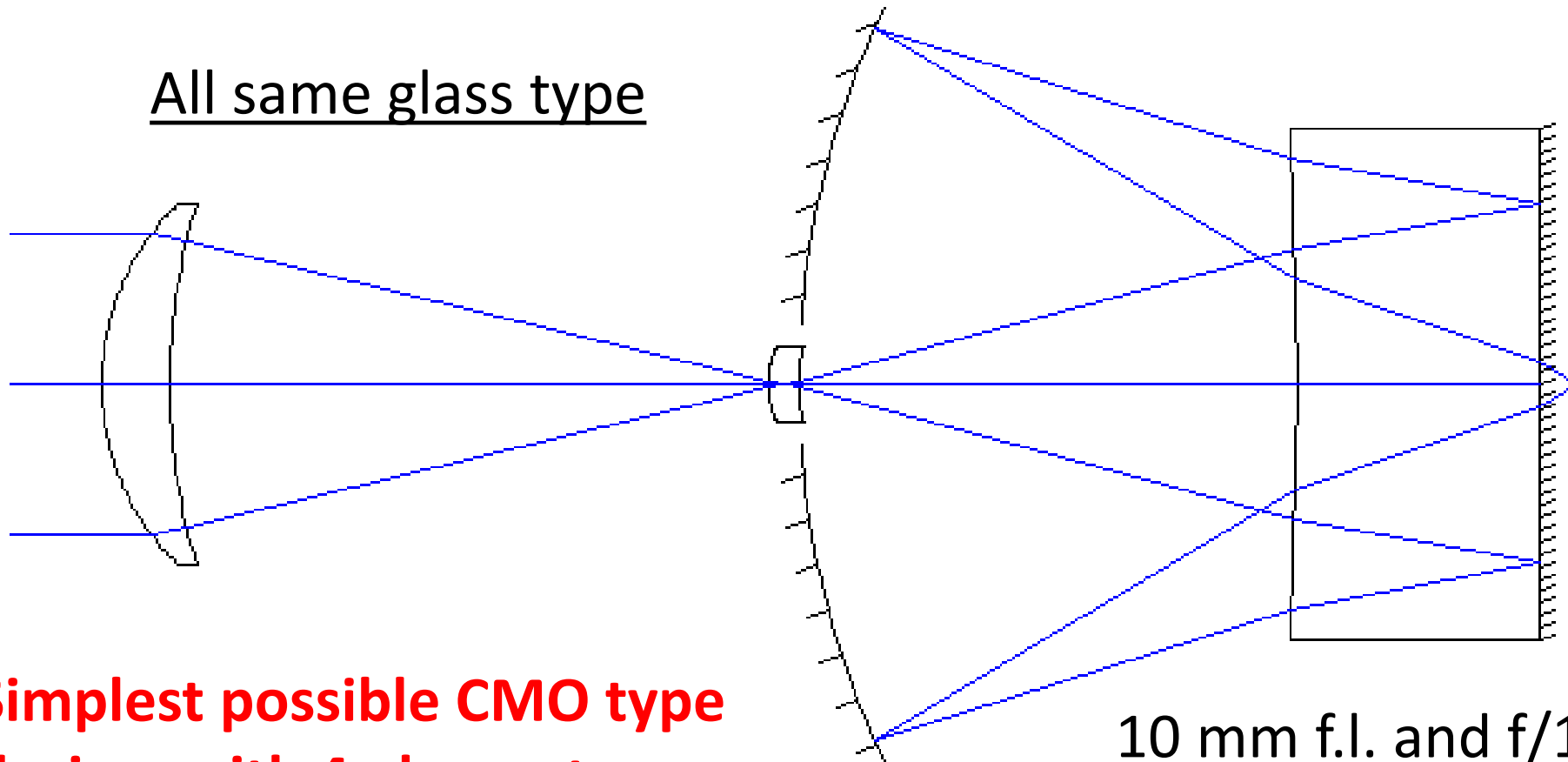
- A key point – the aperture stop was only temporarily located at a place where the theory is simple to understand and the aberration correction method becomes obvious.
- Then later the stop is moved to where it needs to be – like in order to have a telecentric system.
- Once the aberrations are well-corrected they do not change (at the lower-order levels) when the stop is moved.

No name
FOCAL LENGTH = -10 NA = 0.5

UNITS: MM
DES: Shafer

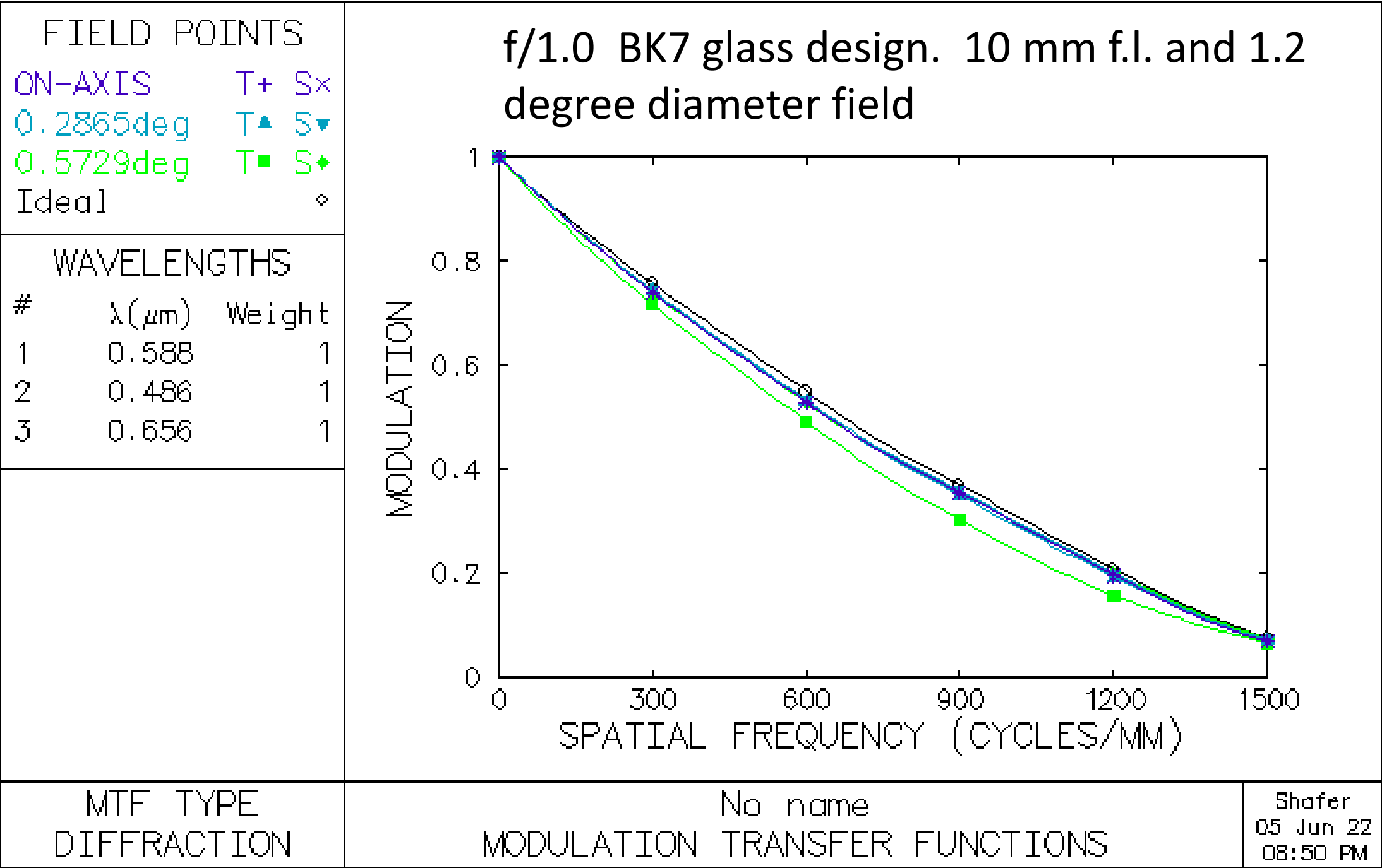
5.76

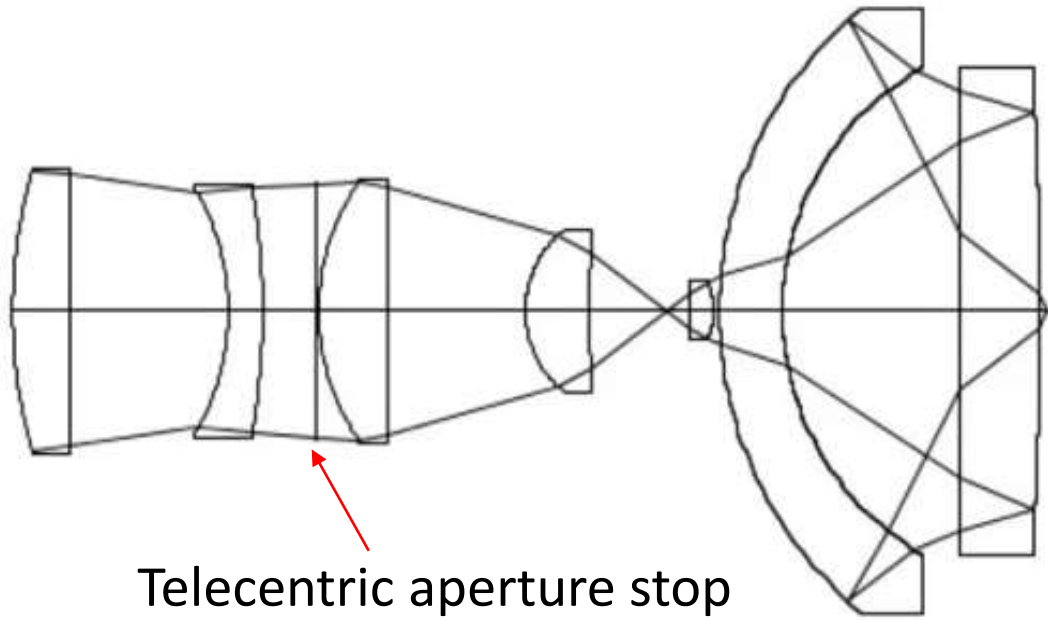
All same glass type



**Simplest possible CMO type
design, with 4 elements**

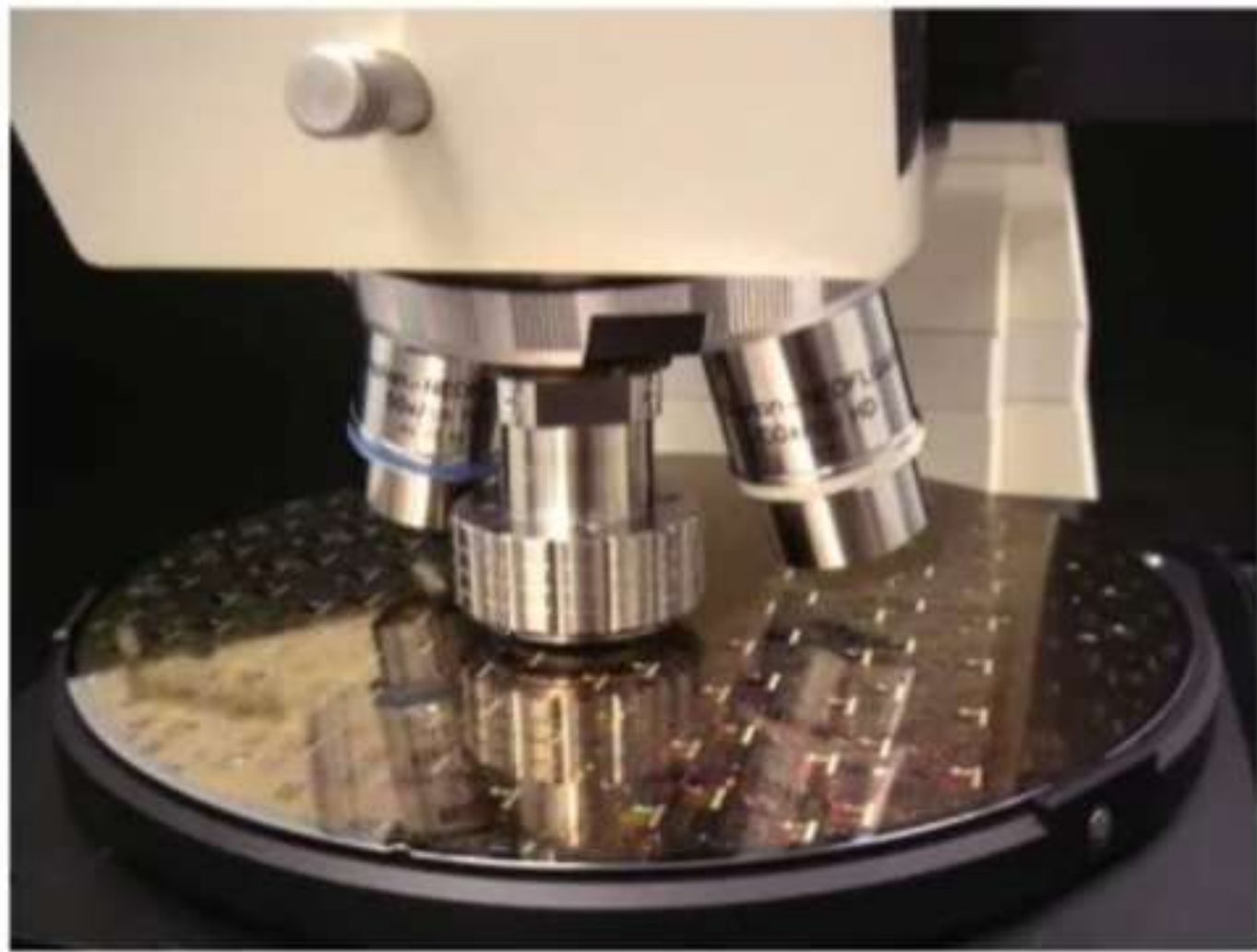
10 mm f.l. and f/1.0
with small field size





Telecentric aperture stop

An example 7 element design corrected from 266-800nm. The diameter of the largest catadioptric element is 25mm. This design has an NA of 0.9 at the object with a field size of 0.13mm. The obscuration is 1.5% of the area.

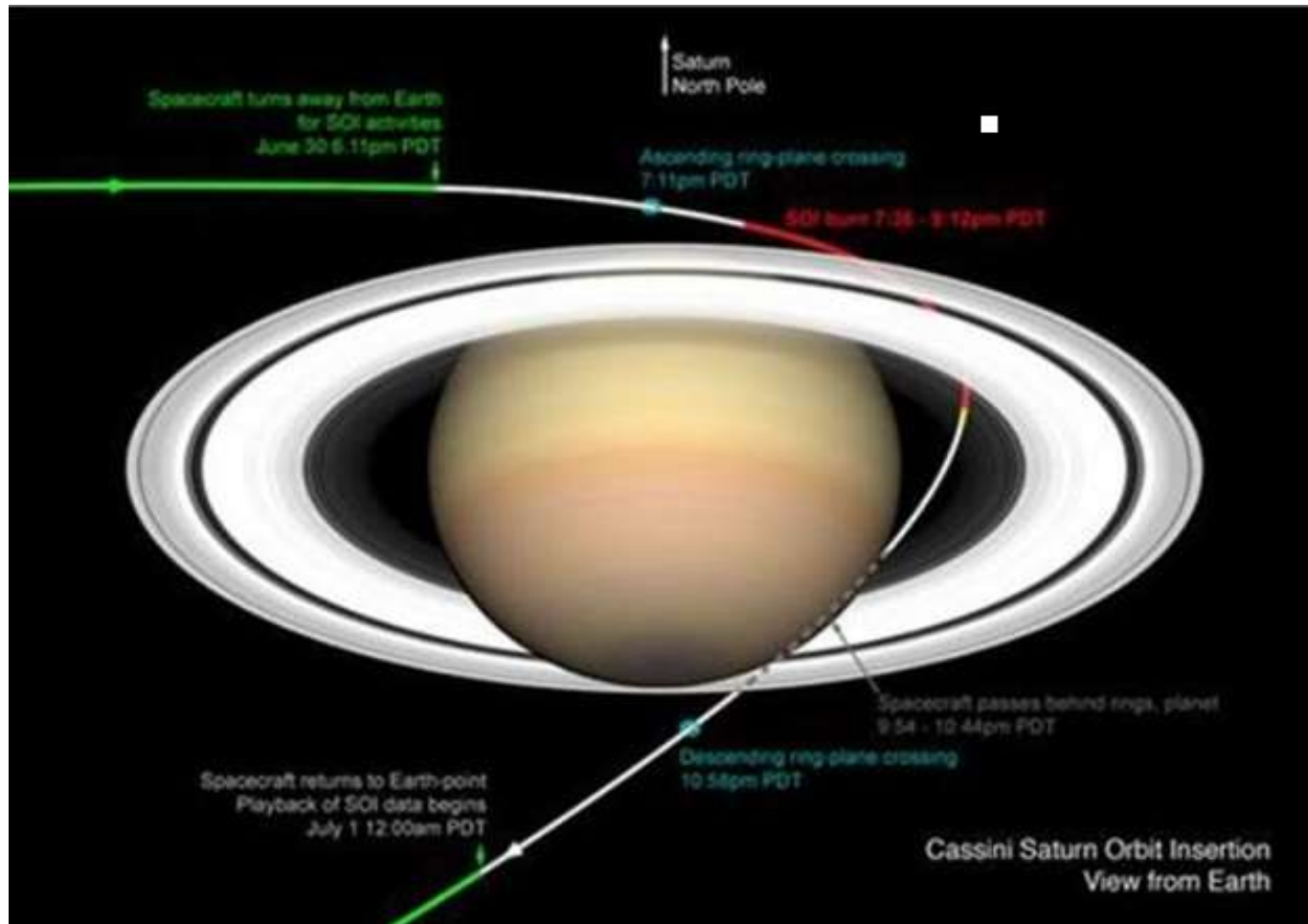


Olympus-made prototype in use.

[Student microscope](#)

High NA well-corrected for an enormous spectral region, .266u to .800u and yet all same glass

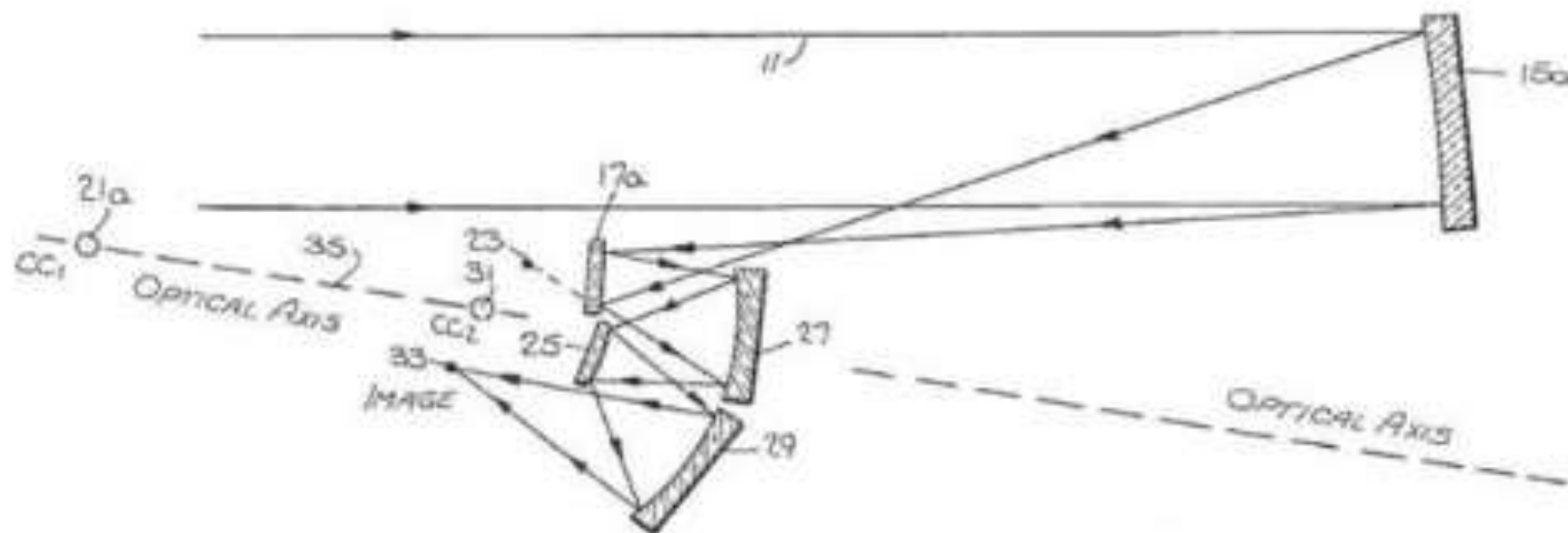
Another example



One of my first patents, in 1977, was for an unusual kind of telescope that only has spherical mirrors.

Many years later one of these unusual telescopes was sent on the Cassini space craft to Saturn.

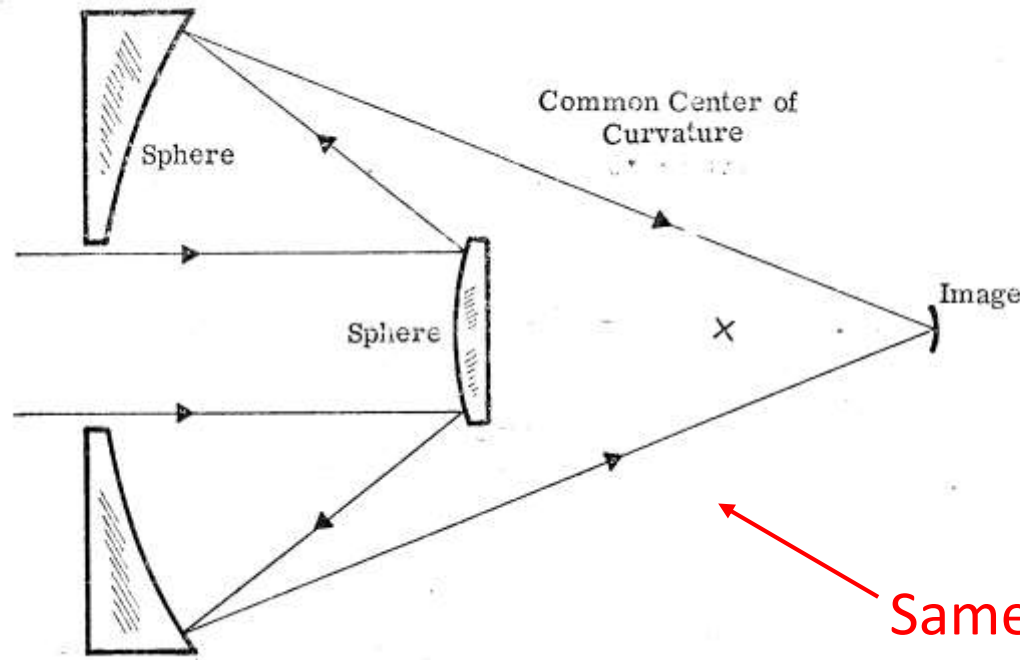
The Cassini mission to Saturn wanted a telescope on-board that was 1) all-reflective, 2) easy to make and align with no aspherics, 3) unobscured, 4) well-corrected over a large field size, and 5) able to become a spectrograph with no extra elements



This drawing from my patent, not to scale, shows the design. What is very unusual is that all the mirrors have their centers of curvature on a single optical axis, unlike other tilted mirrors designs. Also the convex mirror “25” in the drawing is the aperture stop. If this is made a grating surface then the final image is a sharp in-focus spectrum.

Three of these telescope/spectrometers were sent out over the years on three different missions – to Saturn, to the asteroid Vesta and the planetoid Ceres, and to land on a comet.

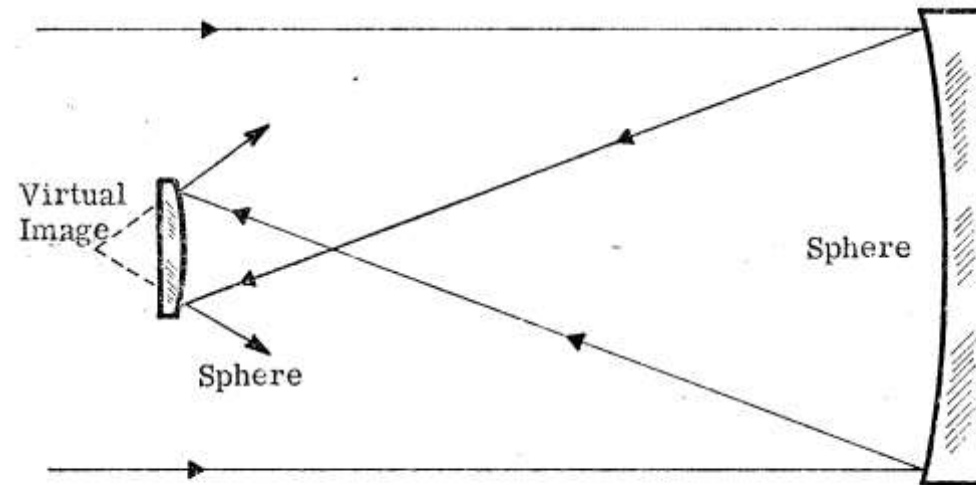
What is the theory behind this design?

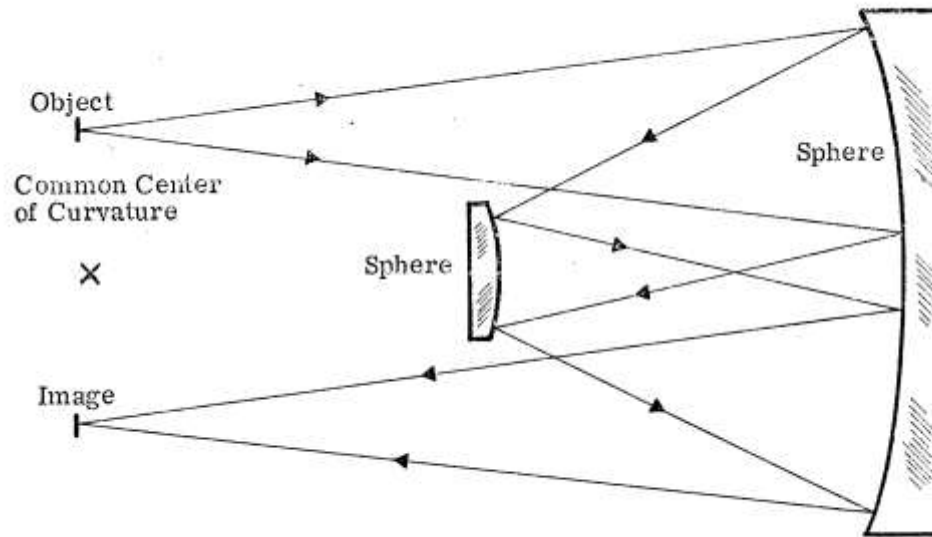


Two concentric spherical mirrors can be corrected for spherical aberration, coma, and astigmatism – with a curved image.

Same design used backwards

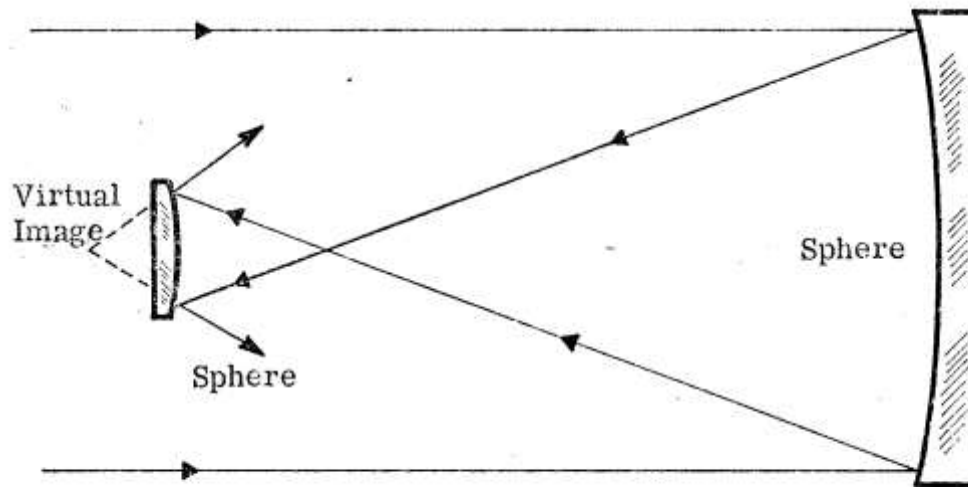
Every concentric system has exactly the same aberrations when used backwards – a peculiar and interesting fact

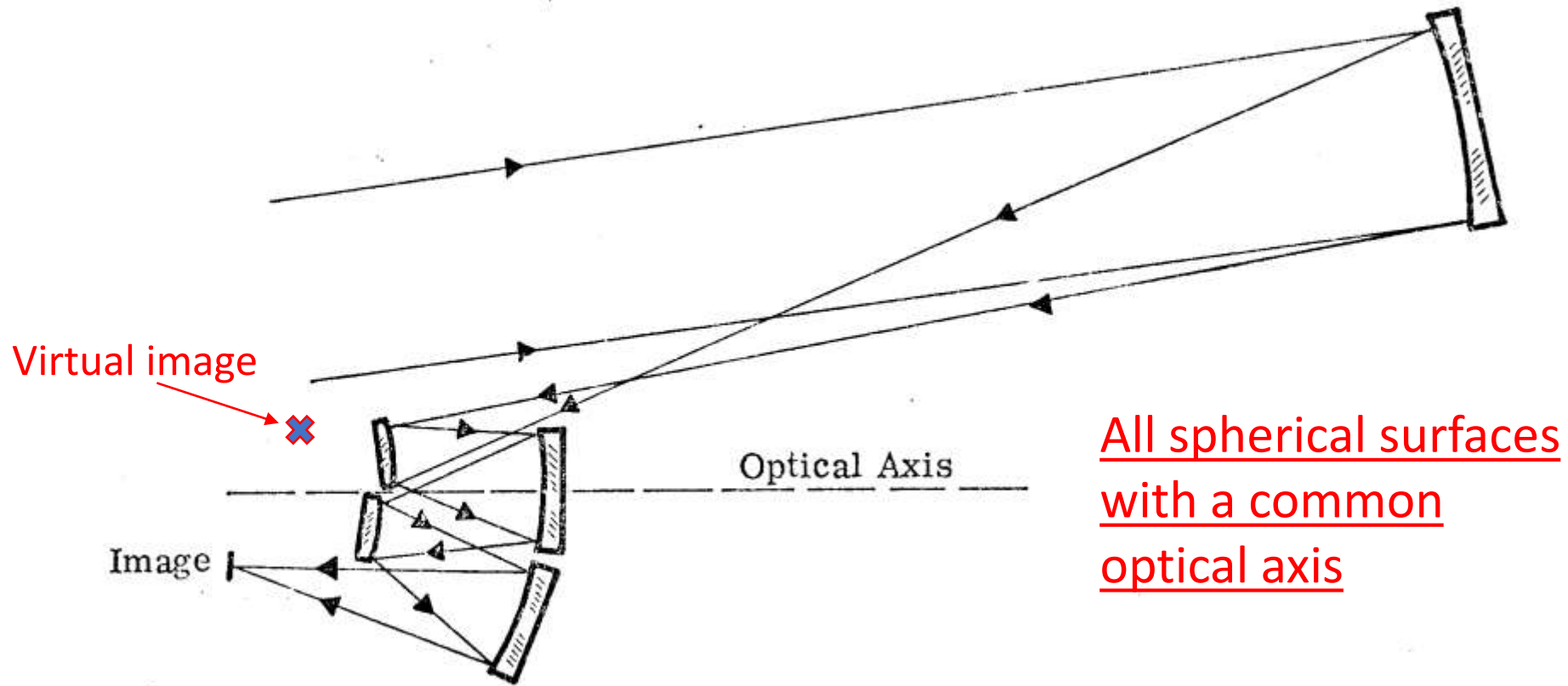




Offner 1X relay design
is well corrected for all
3rd-order aberrations

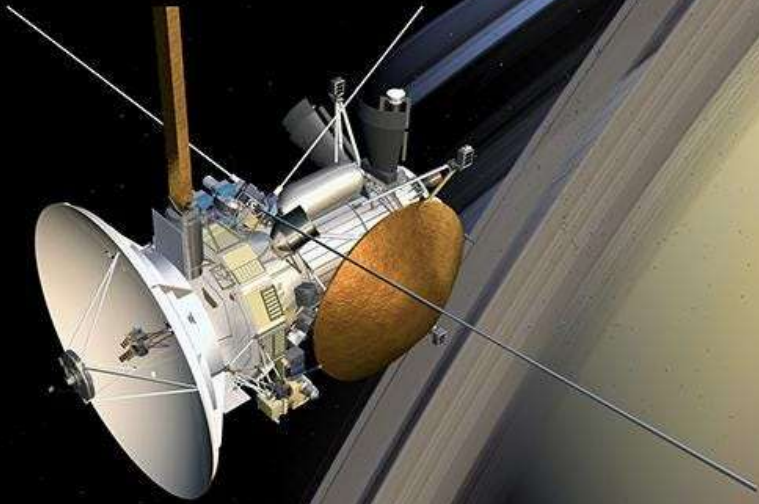
Insight – use this to
relay the well
corrected virtual
image to a well
corrected real image





By putting the field of view to one side of the optical axis we can get an unobscured design. By reoptimizing with all the mirror radii as variables we can correct for Petzval as well as spherical aberration, coma, astigmatism and even distortion.

The Rings of SATURN



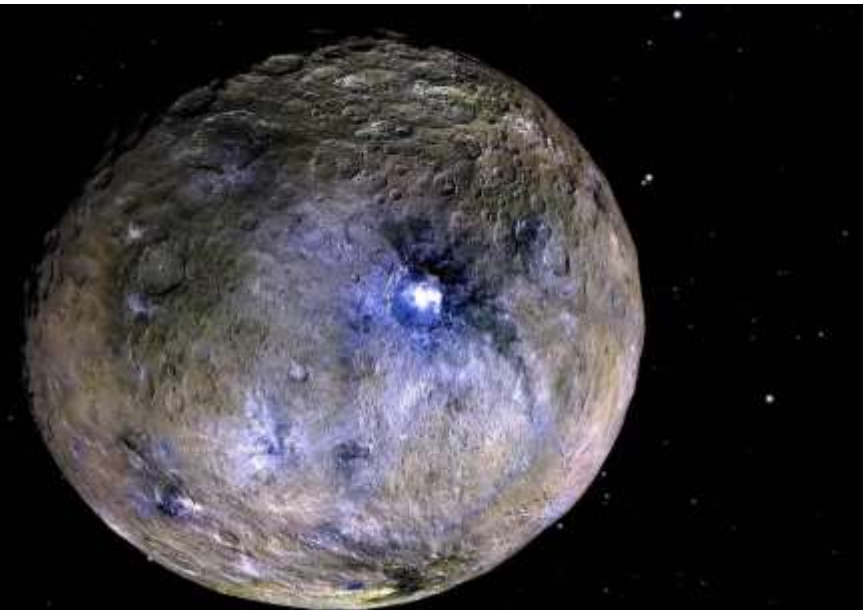
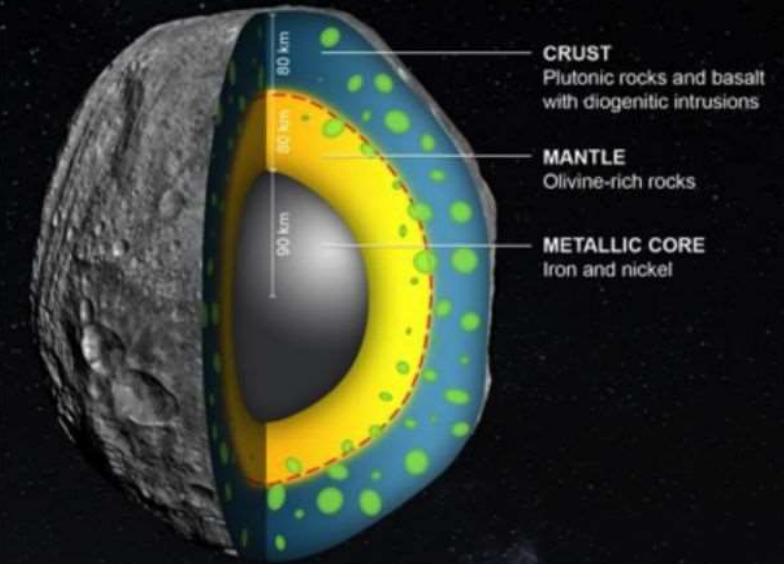
Cassini Space Probe

- Launched in 1997 to orbit Saturn
- Launched the Huygens Probe down to Titan's surface in 2005
- In late 2016, it began a set of extreme orbits around Saturn

Vesta

Ceres

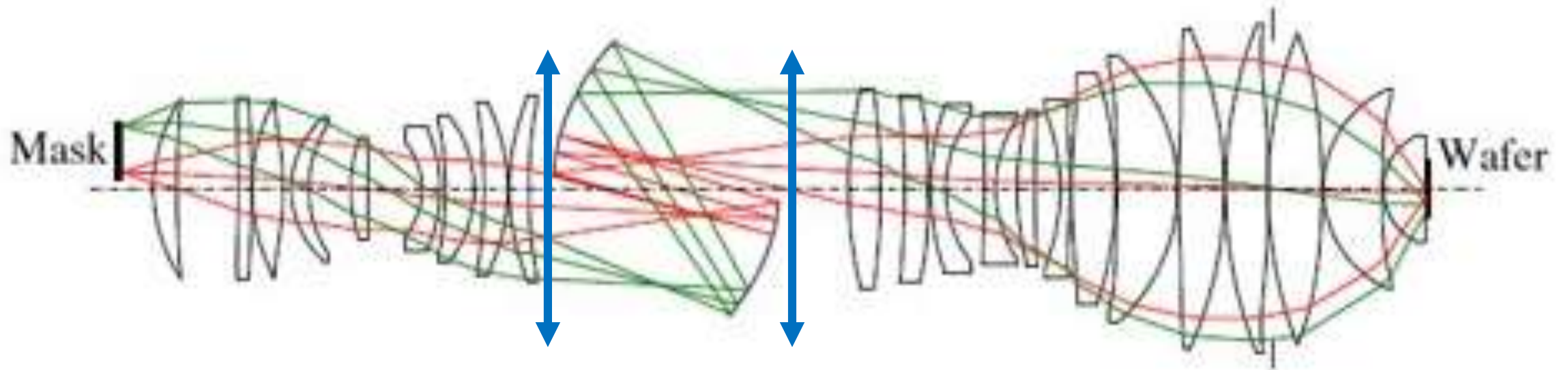
Small planet VESTA



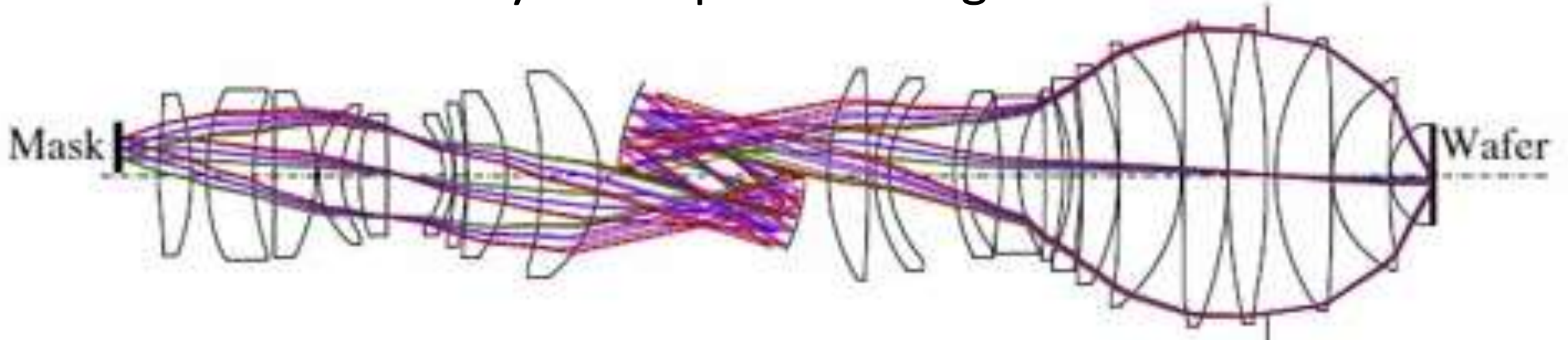


Rosetta
spacecraft
sends
lander to
the surface
of a comet

One more example - a 1.35 NA Chinese immersion design



3 separately optimized (on a curved image) sections. Then the 3 are joined and the whole system optimized together. Result is below here.



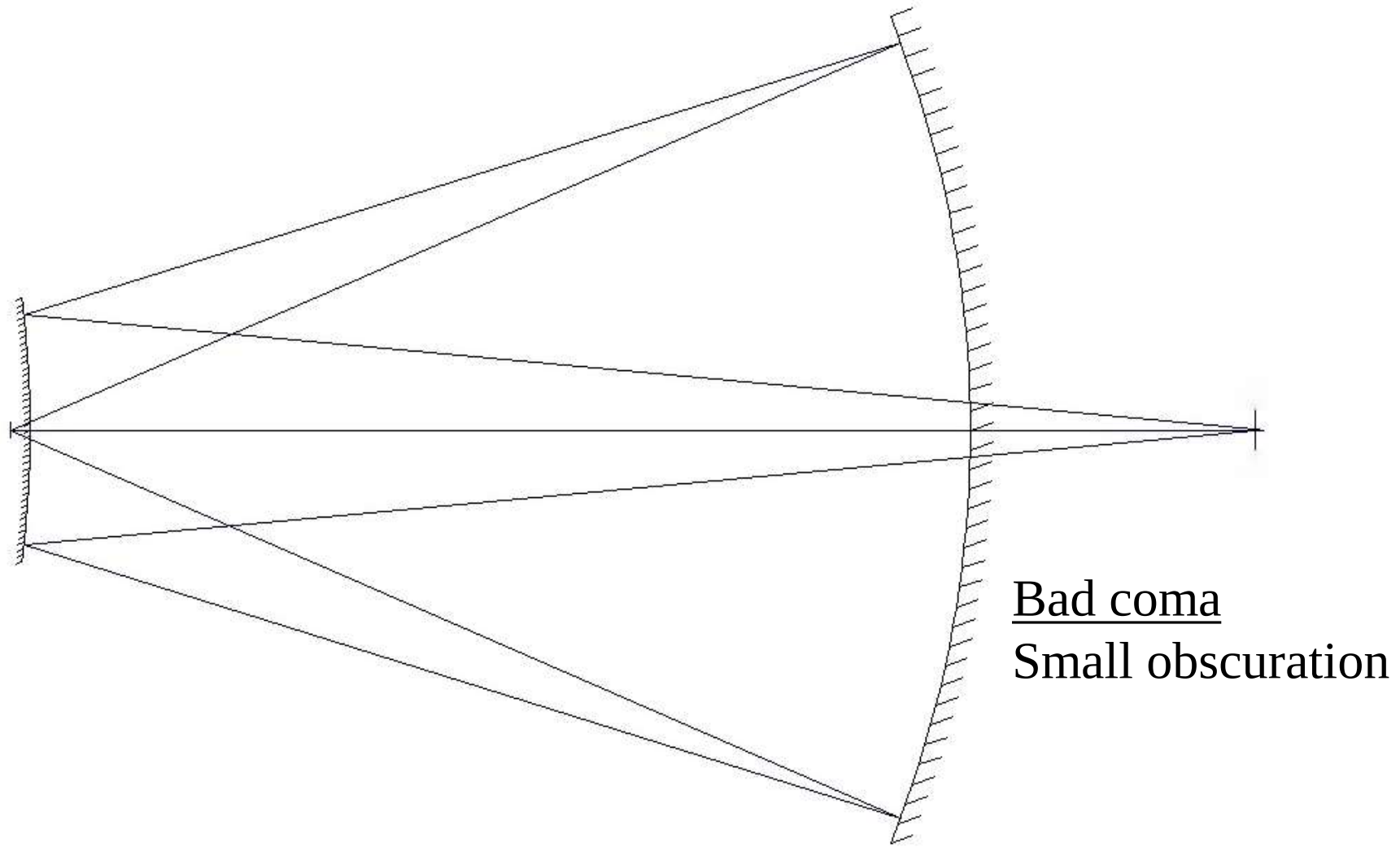
#3

Stop shift theory is very useful
when creating new designs

Example

-

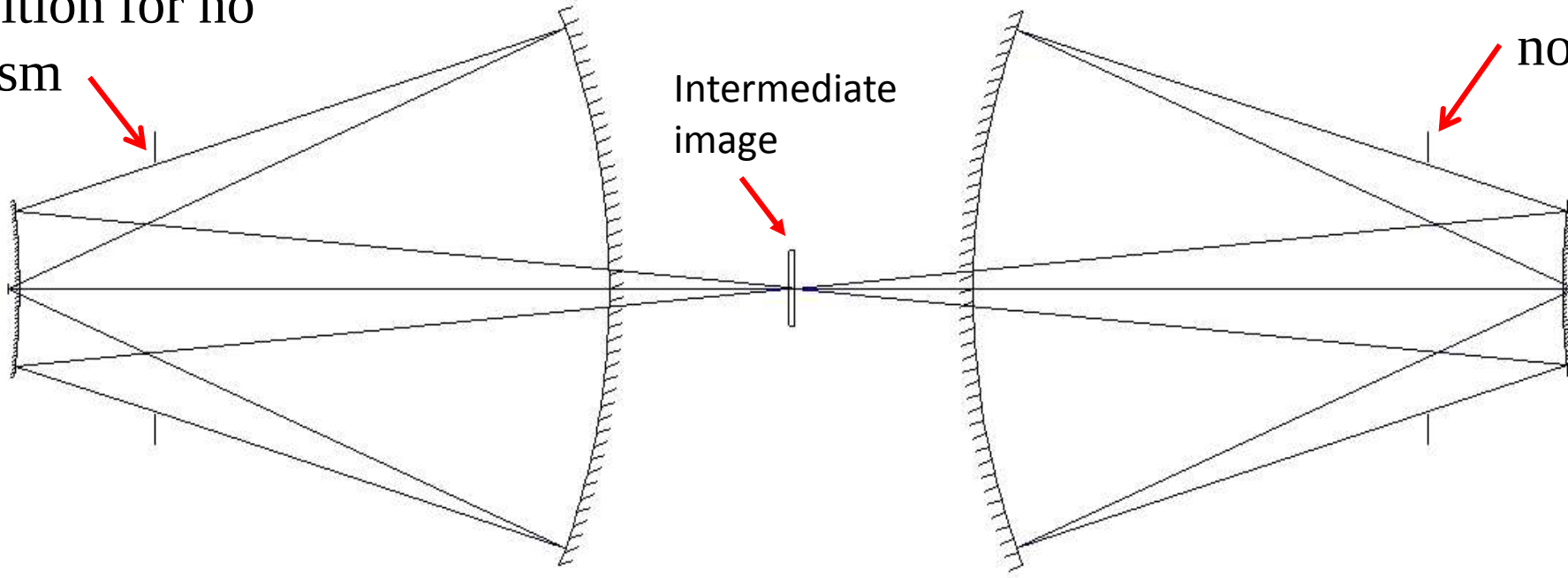
A 1.0X catadioptric relay system
developed using stop shift theory



Spherical mirrors, same radius, corrected for 3rd order spherical aberration

- If a design has spherical aberration then coma is linear with stop position and astigmatism is quadratic with stop position
- If spherical aberration is corrected then coma is constant with stop position and astigmatism is linear with stop position. Then, for non-zero coma, there is always a stop position that corrects for astigmatism.

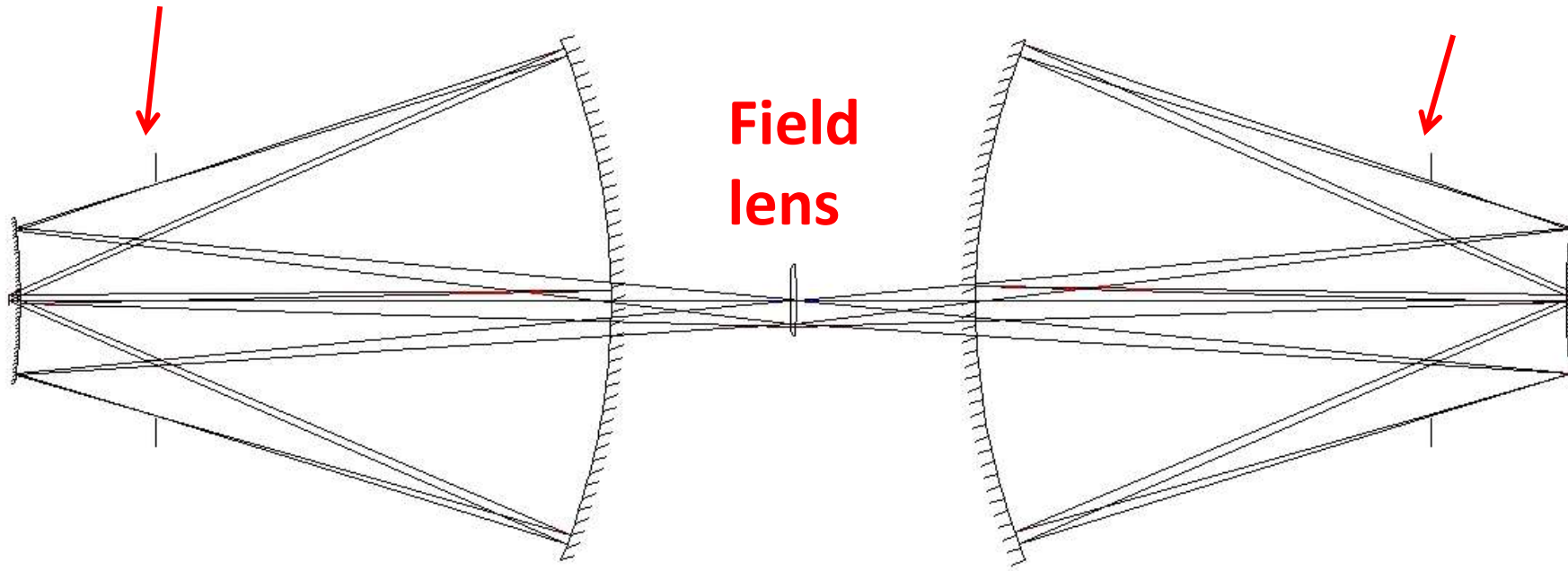
Pupil position for no astigmatism



Pupil position for no astigmatism

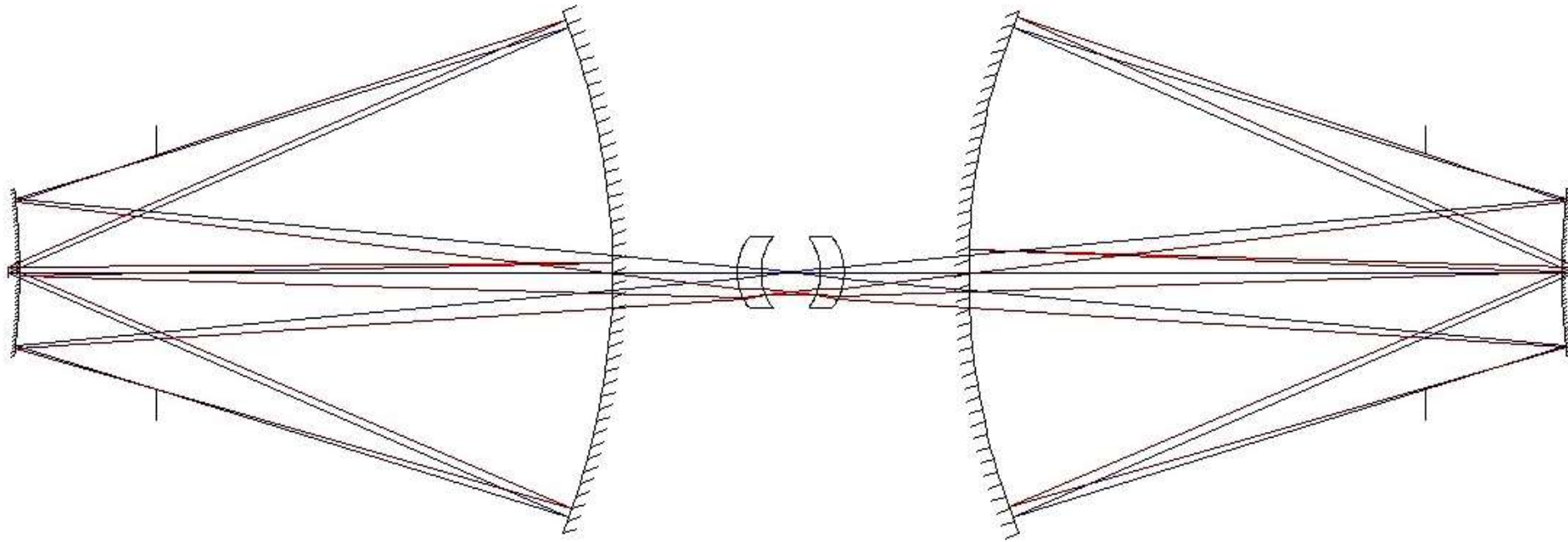
Two symmetrical systems make coma cancel, give a 1.0X magnification aplanat

Each half has a stop position which eliminates astigmatism, since each half has coma. But pupil can't be in both places at the same time.



Astigmatism-correcting pupil positions are imaged onto each other by positive power field lens at intermediate image.

System is then corrected for spherical aberration, coma, and astigmatism, but there is some Petzval from the field lens.



Thick meniscus field lens pair has positive power but no Petzval or axial or lateral color

Result is corrected for all 5 Seidel aberrations, plus axial and lateral color. This shows how a simple building block of two spherical mirrors was turned into something quite useful.

Plus, how stop shift theory is useful for thinking of a new design.

A brief digression

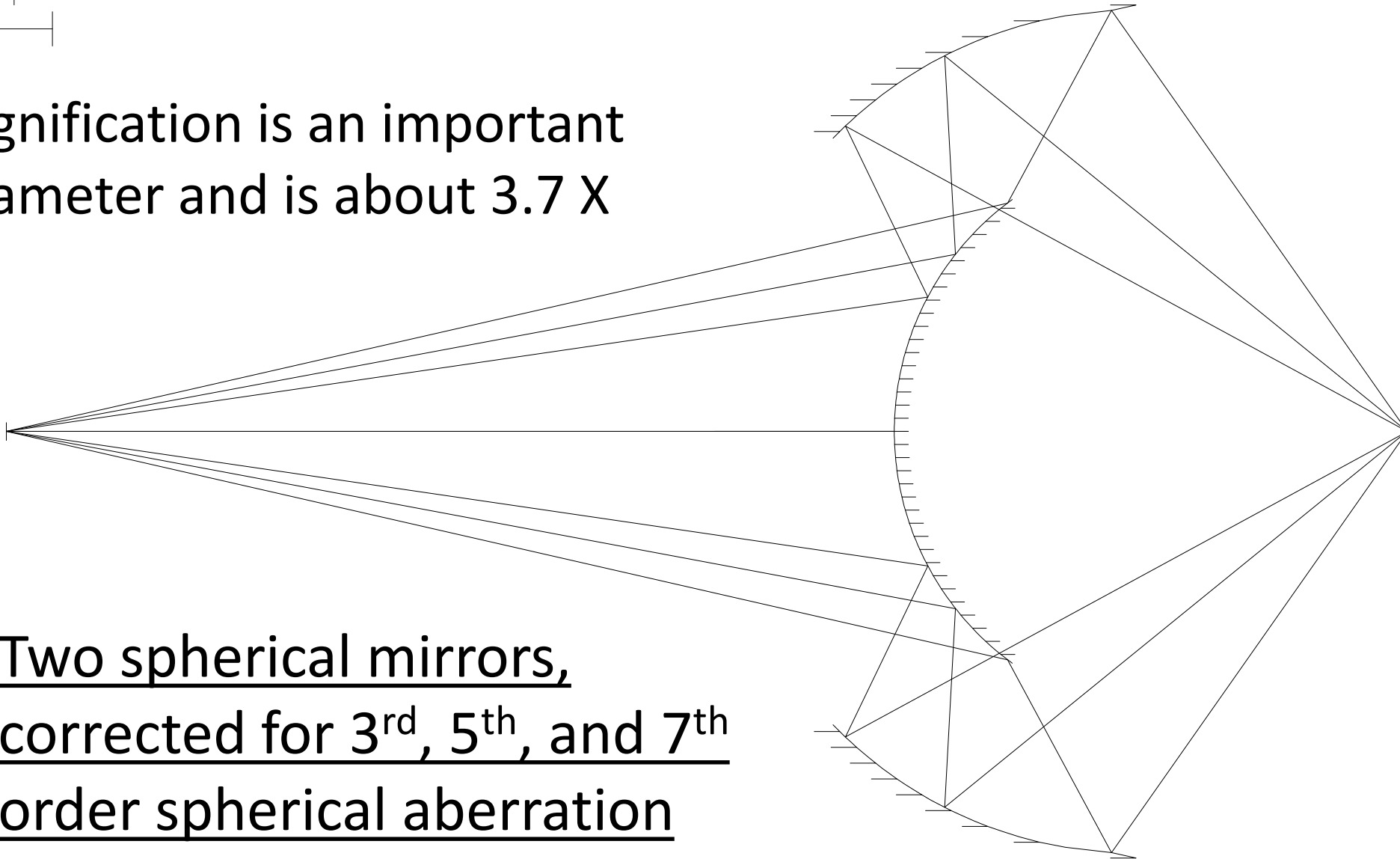
No name
FOCAL LENGTH = 30.32 NA = 0.7

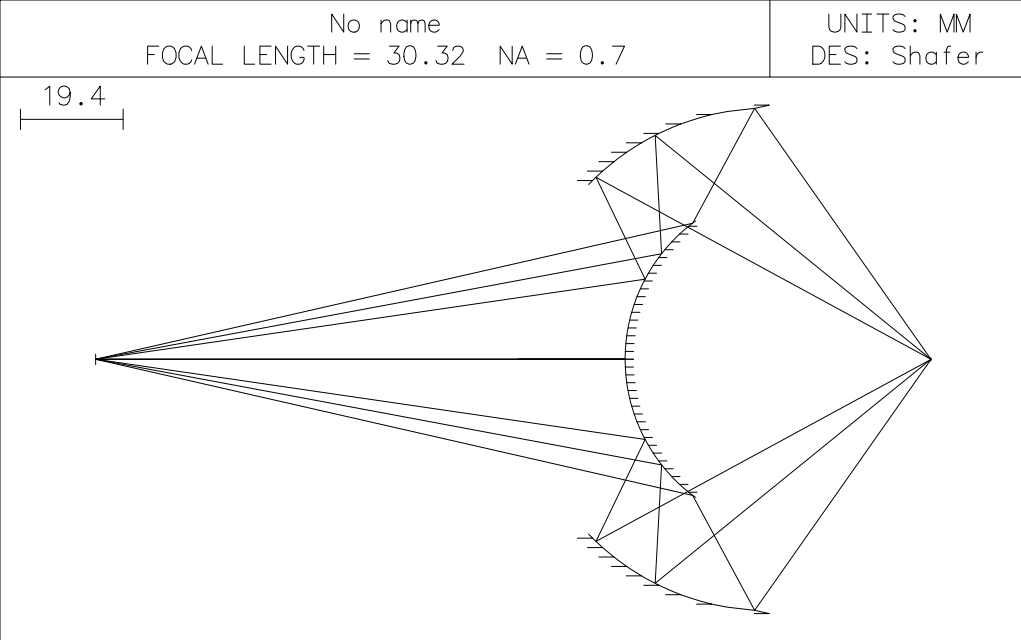
UNITS: MM
DES: Shafer

19.4

Magnification is an important
parameter and is about 3.7 X

Two spherical mirrors,
corrected for 3rd, 5th, and 7th
order spherical aberration





This is a design challenge for both human and AI enhanced computer designers. It is very hard to find this design unless you are right on top of it. Yet it is just two spherical surfaces. It is a good test of design programs.

This design is almost impossible to find, even with a picture like this. The reason is that in this design both of the spherical mirrors have a very large amount of spherical aberration, of opposite signs and they cancel almost exactly to high orders – if you have this exact configuration. If you have a design starting point that is close to the good solution, but not right at it, the cancellation is not complete. The computer will “see” that the easiest way to reduce that difference of the two large numbers is to minimize both numbers. So it immediately heads for the two trivial 1.0X solutions of a flat mirror and a mirror concentric about the rays, where both mirrors have zero aberration.

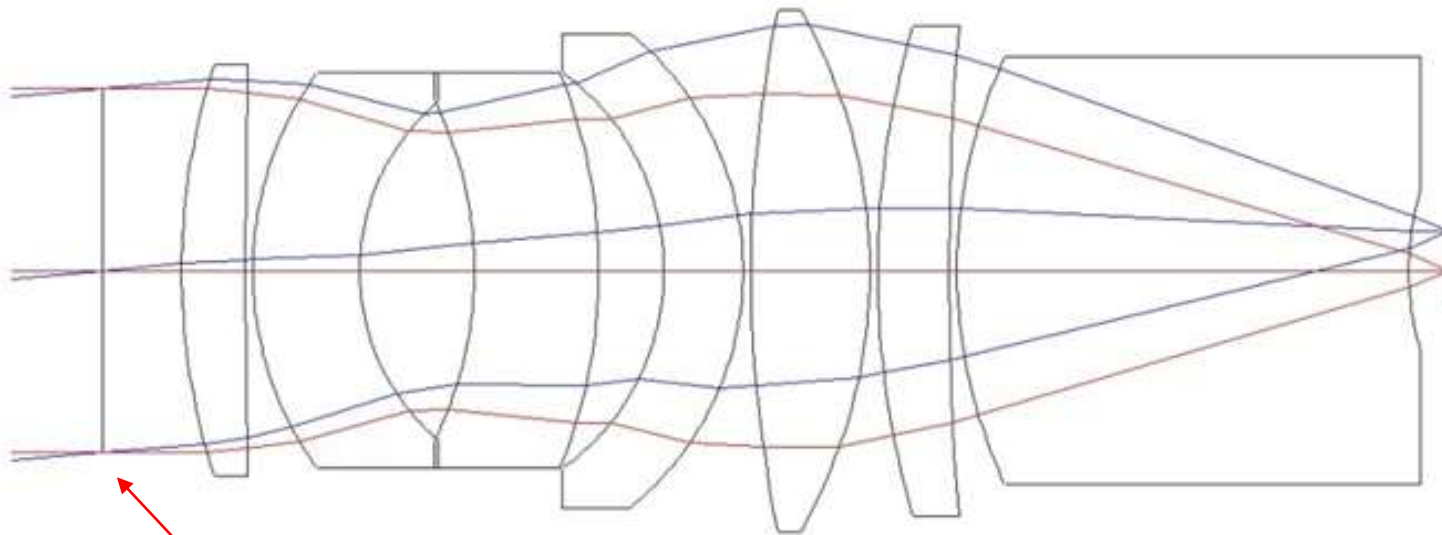
Another example of using stop shift theory

all silica, .266u
FOCAL LENGTH = 57.51 NA = 0.3999

UNITS: MM
DES: OSLO

20.2

All fused silica glass



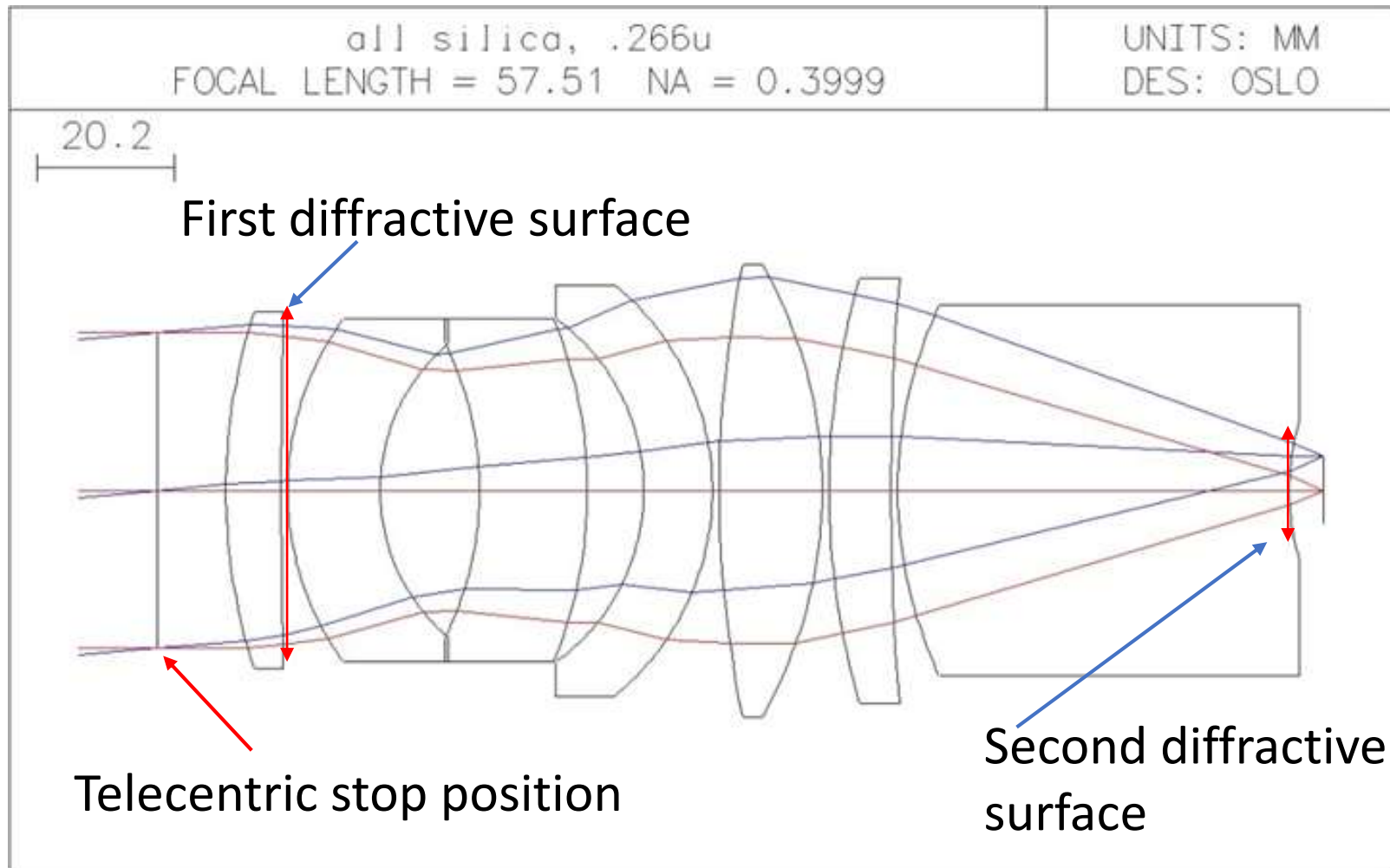
Telecentric stop position

Here is a monochromatic deep UV design that is well corrected at .266u

Suppose we want to correct it for axial and lateral color. We could add some calcium fluoride lenses to correct for color but their small dispersion difference with silica requires strong and thick lenses.

Instead we will consider using diffractive surfaces, which are highly dispersive. But they have some scattering transmission losses.

Another example of using stop shift theory



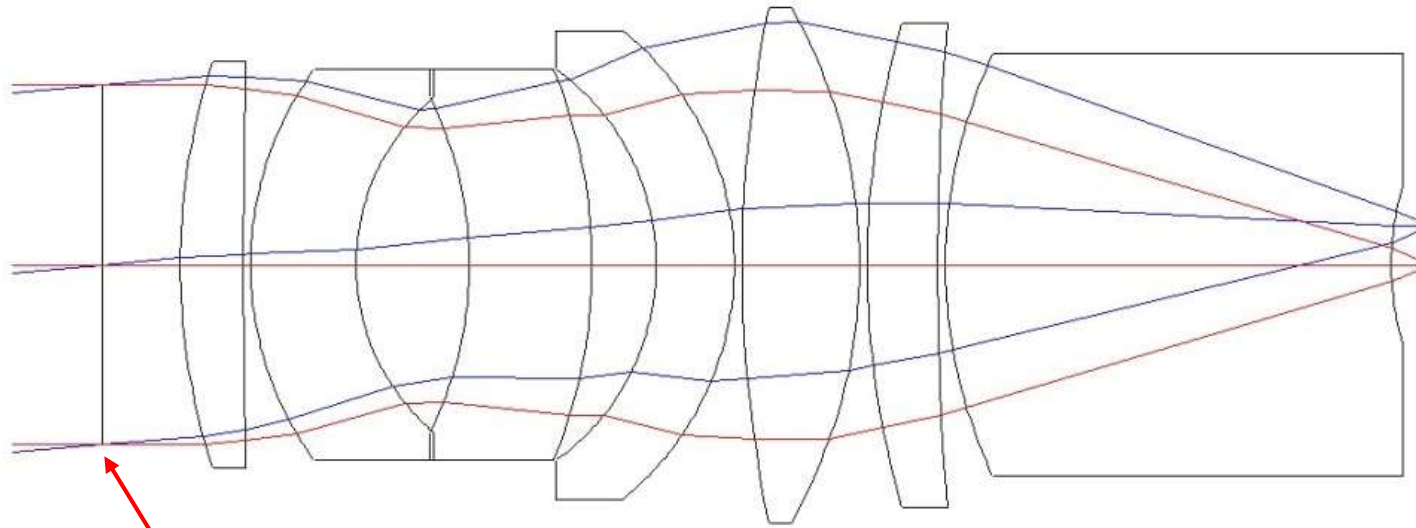
Two widely separated diffractive surfaces with appropriate powers can correct both axial and lateral color of this design. There are many possible positions in the design which work well. Here I show a random example. But costs and extra scattering would make it better to use just one diffractive surface. How then could both axial and lateral color be corrected? I'm glad you asked.

all silica, .266u
FOCAL LENGTH = 57.51 NA = 0.3999

UNITS: MM
DES: OSLO

20.2

Telecentric design



stop

All same glass type

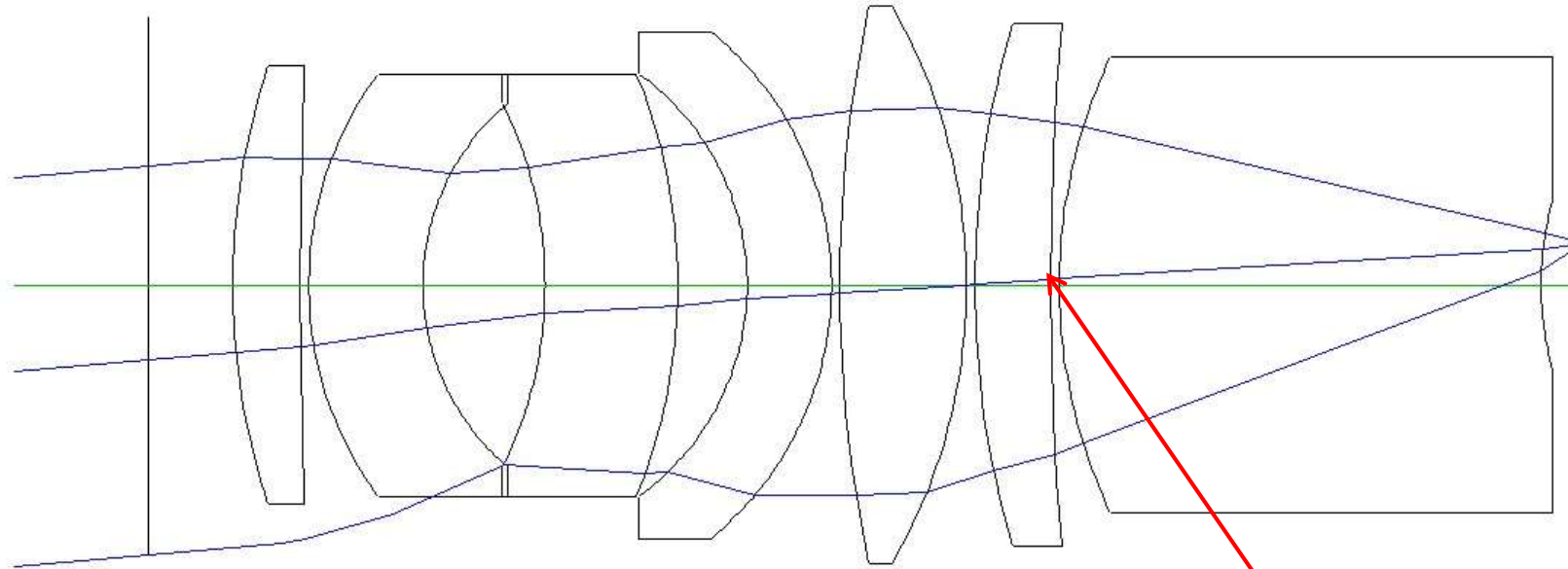
Here is the plan

- Lateral color depends on aperture stop position, since axial color is not corrected.
- Move the stop around and find out what temporary position makes **lateral** color be zero.
- Then correct **axial** color at that location. Let's try using a diffractive surface.

all silica, .266u
FOCAL LENGTH = 57.51 NA = 0.3999

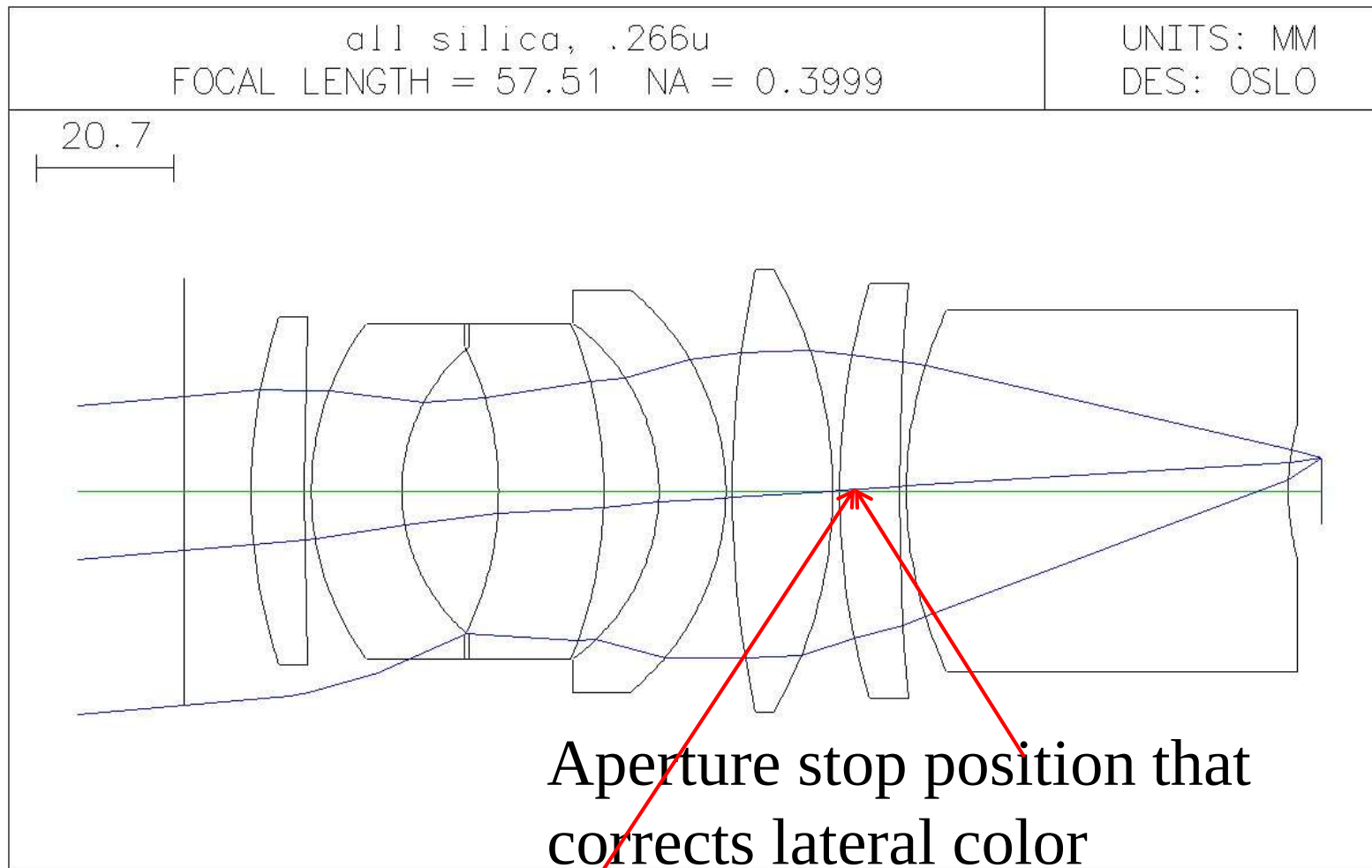
UNITS: MM
DES: OSLO

20.7



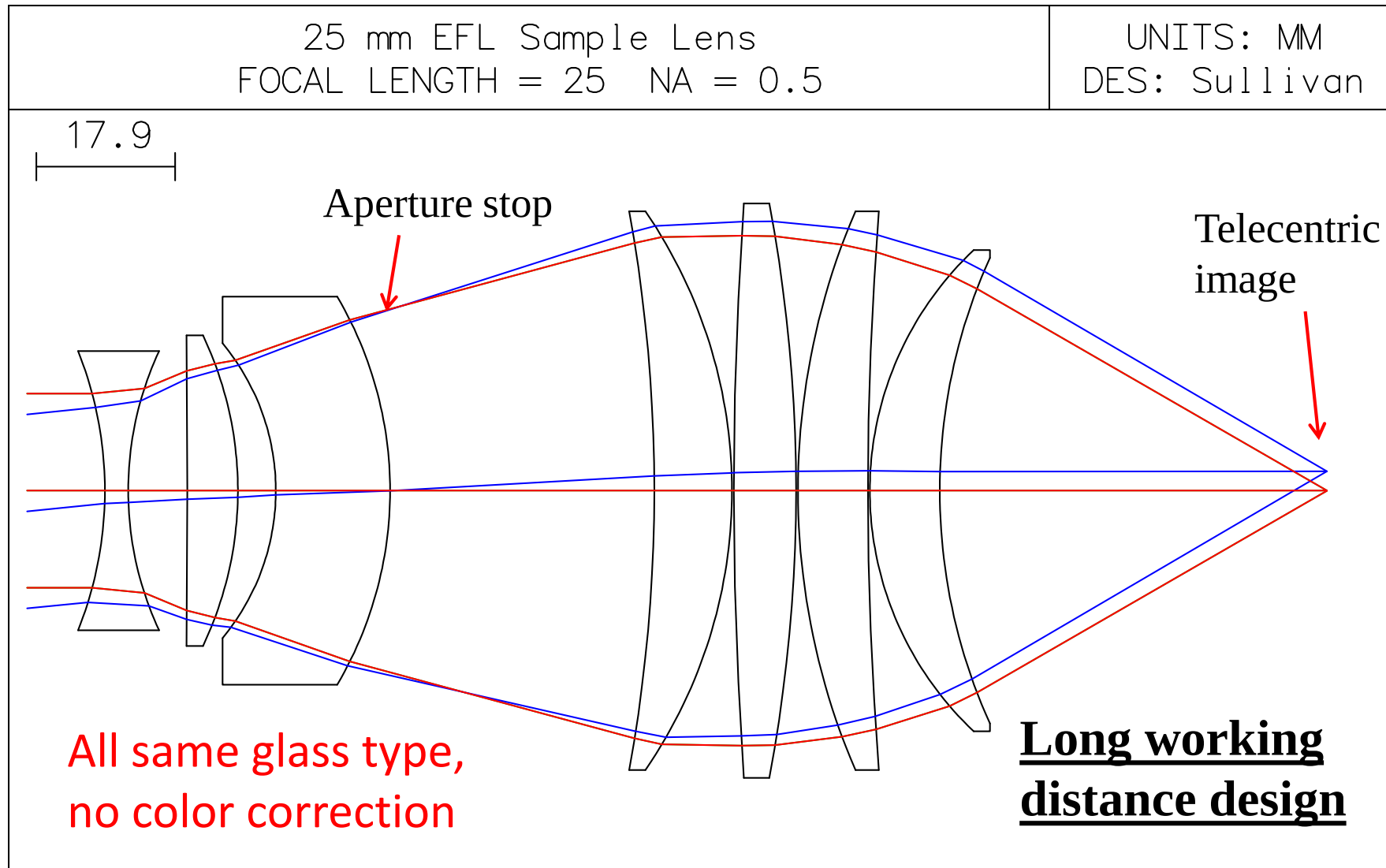
Aperture stop position that corrects lateral color

We move the stop position back and forth until we get **lateral** color = zero



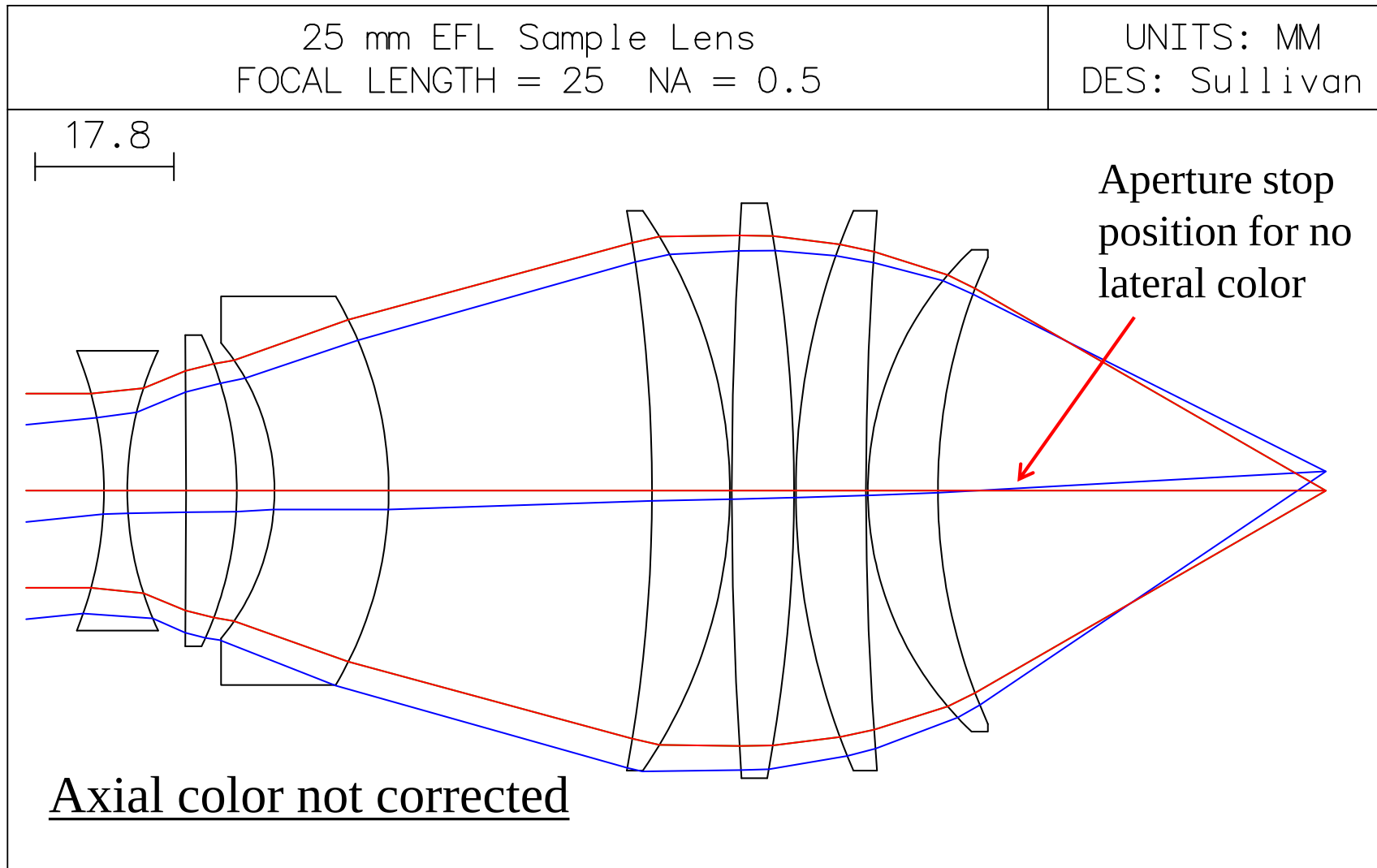
If we correct axial color here, with a diffractive surface, then both axial and lateral color will be corrected. Then we can move the stop back to where we want it, and **both color types will still be corrected.**

- This same design method indicates where to add lenses (instead of diffractive surfaces) for color correction
- It minimizes the number of extra lenses needed for color correction
- But it may indicate adding color correcting lenses where we don't want them, because of space constraints
- Then we rely on conventional color correcting techniques

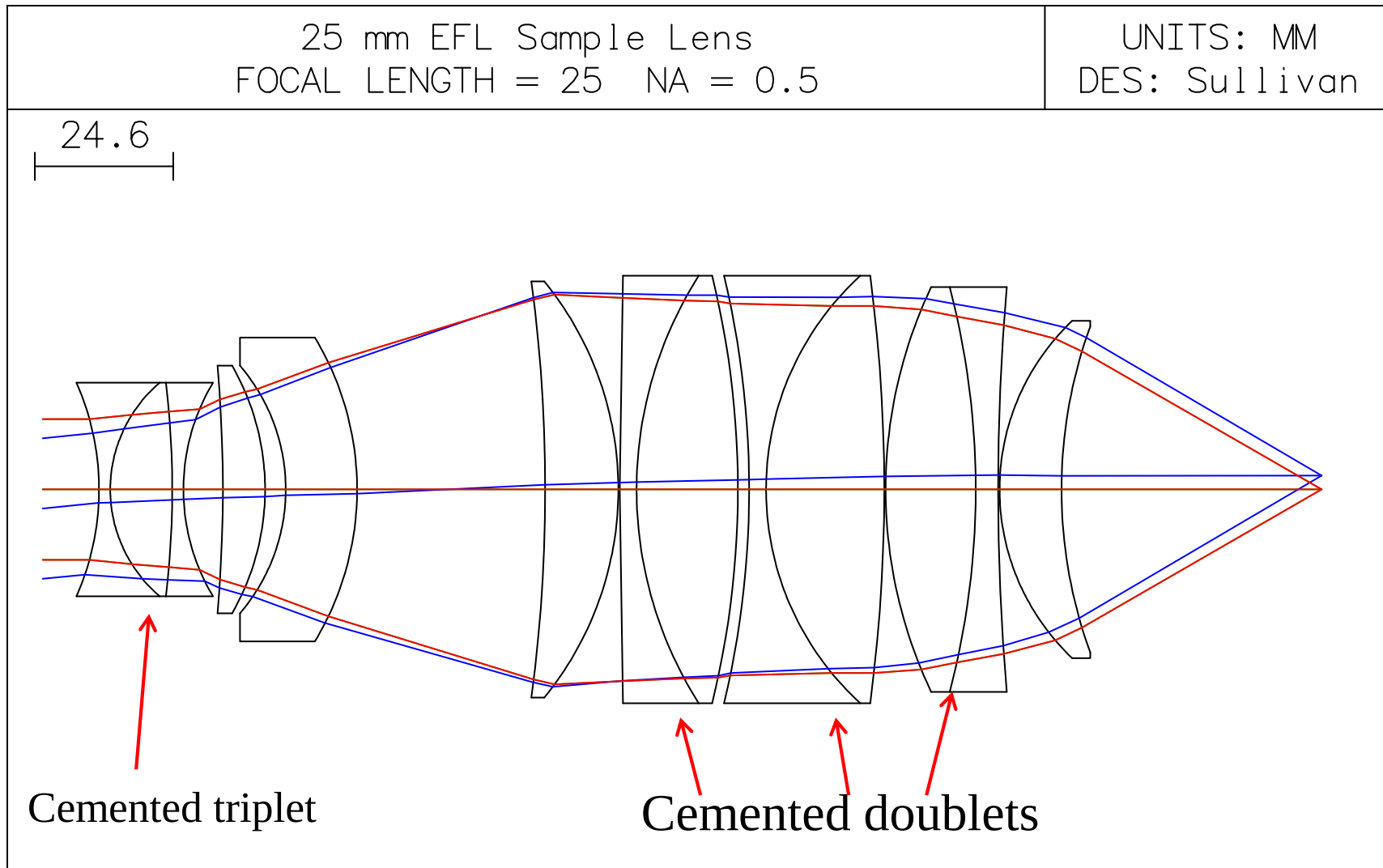


Diffraction-limited monochromatic f/1.0 design with 5.0 mm field diameter

[Here is another example](#)



Aperture stop position for no lateral color may not be in a desirable, place - as in this long working distance design. We don't want to put axial color correcting lenses there, in the long working distance space.



In these cases you have to use two separated groups of color correcting lenses, instead of just one, for axial and lateral color correction. That makes for a more complex design like here where I show a deep UV design using silica and calcium fluoride lenses.

Conclusion

- Stop shift theory gives insight into the aberration theory of a design and also suggests new design possibilities
- Temporary stop shift is a powerful design tool and does not usually require changing the actual final position of the stop, which may be set by the telecentric condition or other constraints

#4

Temporary use of aspherics during design optimization is a very powerful way to find new designs and improve existing ones.

Example – a 2X monochromatic lens relay



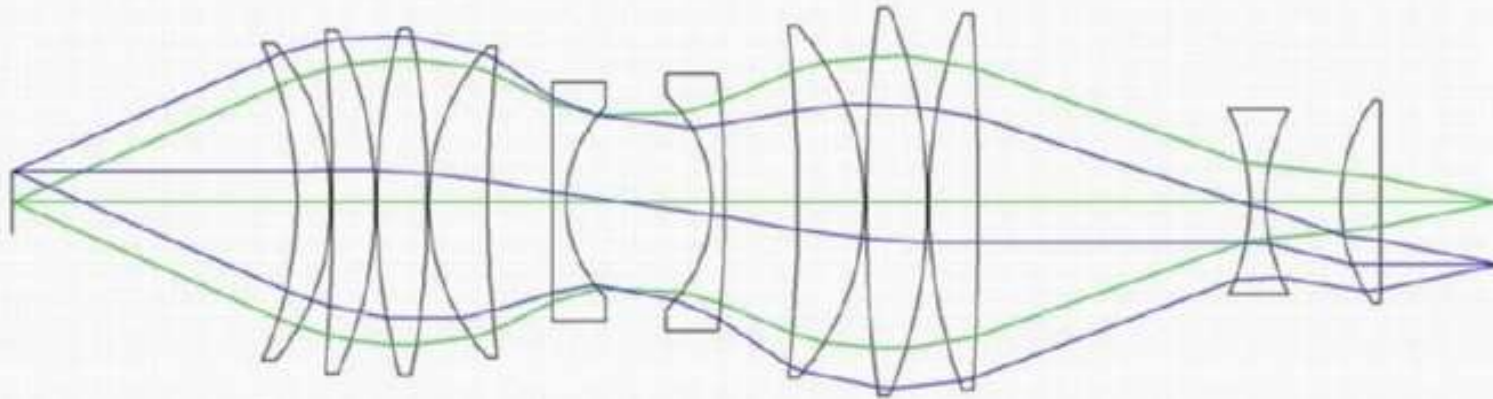
What is the quickest way to go from New York to Munich? By plane, of course. Try to get to the departure gate on time. But you don't need a plane when you are within New York City or when you are within Munich. You only need it to go from one place to the other. In a similar way the use of aspheric surfaces during the design process can ease the path of a design from one solution region to a better one, and yet once there the aspherics can then often be removed as no longer needed, by a certain method.

Even simple designs can have multiple good solution regions and complex designs have very many more. Usually good solutions are separated from nearby other good solutions by regions of bad correction and it is hard for optical design programs to move through the bad regions – especially if you start in a good region where the design would have to get worse first before it then gets better in a nearby good solution. Design programs are set up to optimize a design, always making it better, not let it first get worse on a route to a better solution. Adding aspheric surfaces to a design can allow it to more freely move around in solution space because they simulate adding several new lenses to a design, giving lots more variables to work with. But the aspherics might only be needed as a temporary aid to the optimization process and can then usually be removed once a new good solution has been found.

2X relay, monochromatic
FOCAL LENGTH = 341.7 NA = 0.2

UNITS: MM
DES: OSLO

55.6



The design's wavefront is .042 waves r.m.s. or better over its image size but we want better to allow for tolerances in making it.

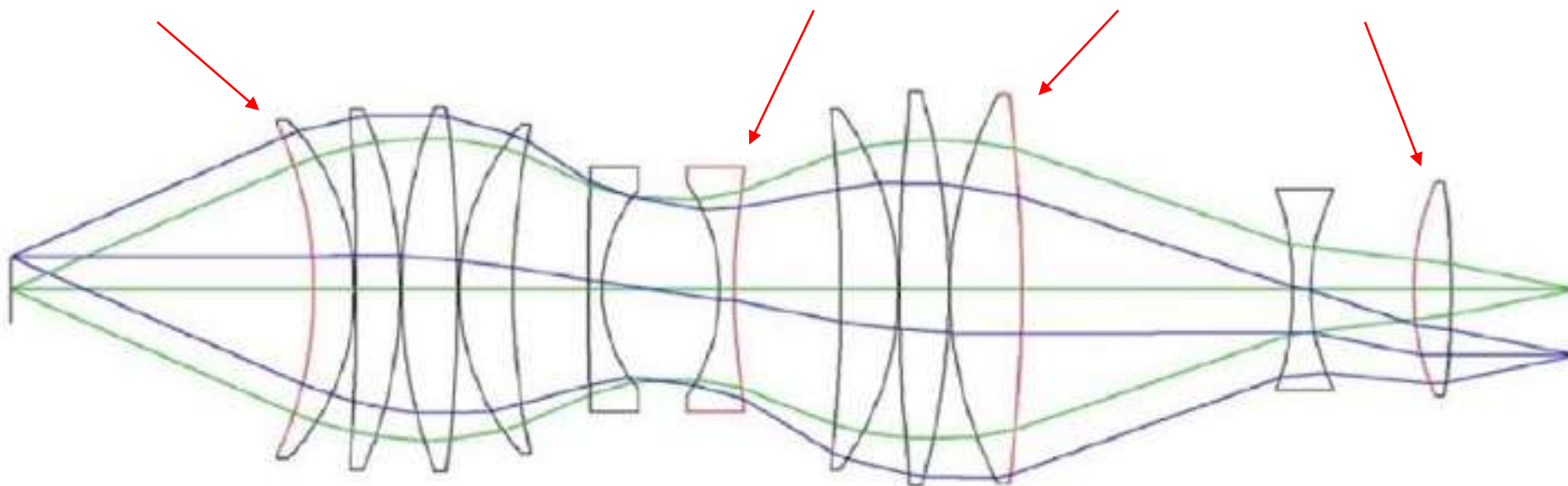
Here is a well optimized good existing design that we want to make better, with better image quality. Making a spherical lens surface be aspheric is often equivalent to adding two new lenses to the design, giving a lot more means to correct aberrations and find a better solution region. Let's add to this design aspheric surfaces at the front and back of the design and 2 more in the middle and then reoptimize. That is equivalent to adding many new lenses to the design.

2X relay, monochromatic
FOCAL LENGTH = 608.8 NA = 0.2

UNITS: MM
DES: OSLO

55.6

4 Aspherics added as new additional design variables

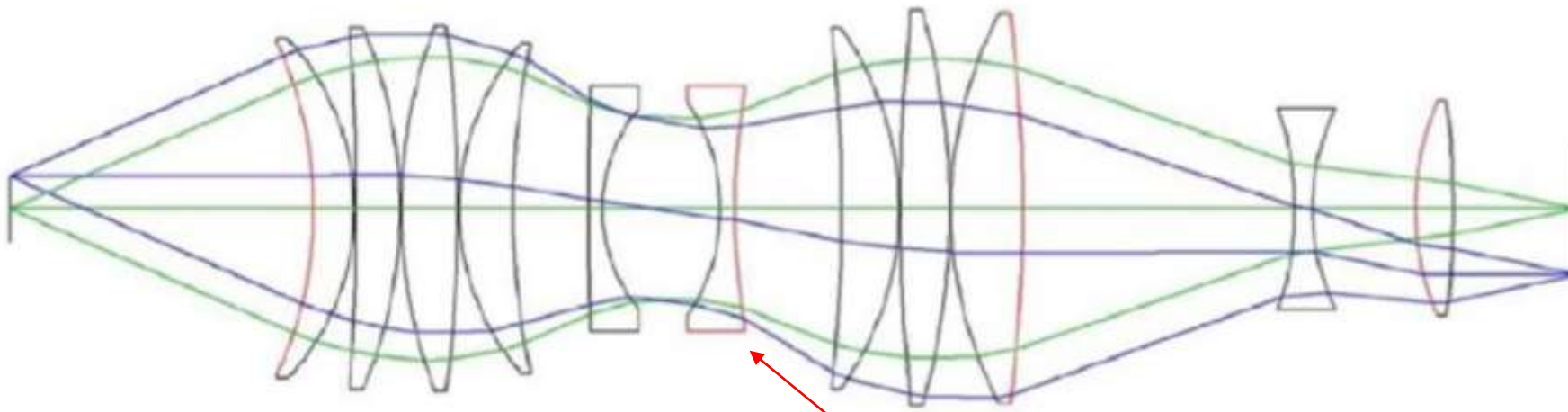


With these 4 aspherics added at the front, back and middle of the design we then reoptimize using the aspheric coefficients as new variables in the optimization. The worst image quality over the field then drops down to .014 waves r.m.s., or **3X better** than before. The design still looks the same.

2X relay, monochromatic
FOCAL LENGTH = 608.8 NA = 0.2

UNITS: MM
DES: OSLO

55.6



So all the improvement in the design is due to the two middle aspherics, not the two end ones, which can be removed.

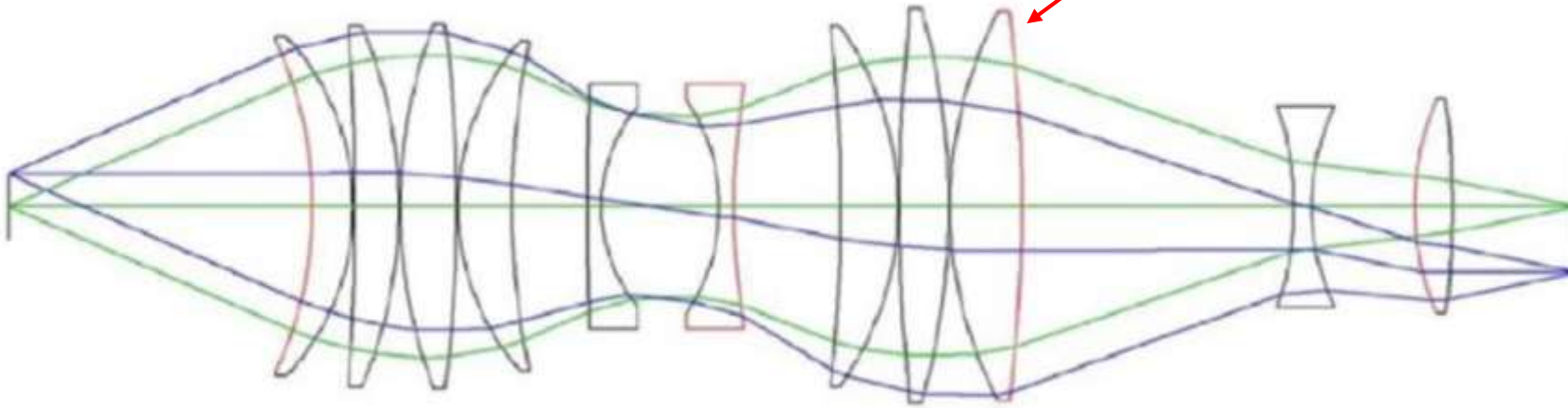
Then we try not using the aspheric in the front of the design but just the two middle ones and the back one and find that reoptimization gives just as good as before – about .014 waves r.m.s. image quality over the field. The same good result happens if you keep the first 3 aspherics and leave out the last one. So there is not any point in splitting lenses in the front or back sides of the original all spherical surface design. This experiment here has shown us that.

2X relay, monochromatic
FOCAL LENGTH = 608.8 NA = 0.2

UNITS: MM
DES: OSLO

55.6

Best single aspheric position



Then we find that either of the two middle aspherics can give almost all the performance improvement. The aspheric indicated here is the better of the two and with just this one aspheric in the design the correction is .016 waves r.m.s. over the field instead of .014 waves r.m.s. with all four aspherics and .042 with none.

This is typical – most designs have just one part of the design where an aspheric or splitting lenses is very beneficial. But we don't know where that position is. This process just shown allows us to easily find out where.

2X relay, monochromatic
FOCAL LENGTH = 372.6 NA = 0.2

UNITS: MM
DES: OSLO

55.6

Design with **no aspherics** and one new lens

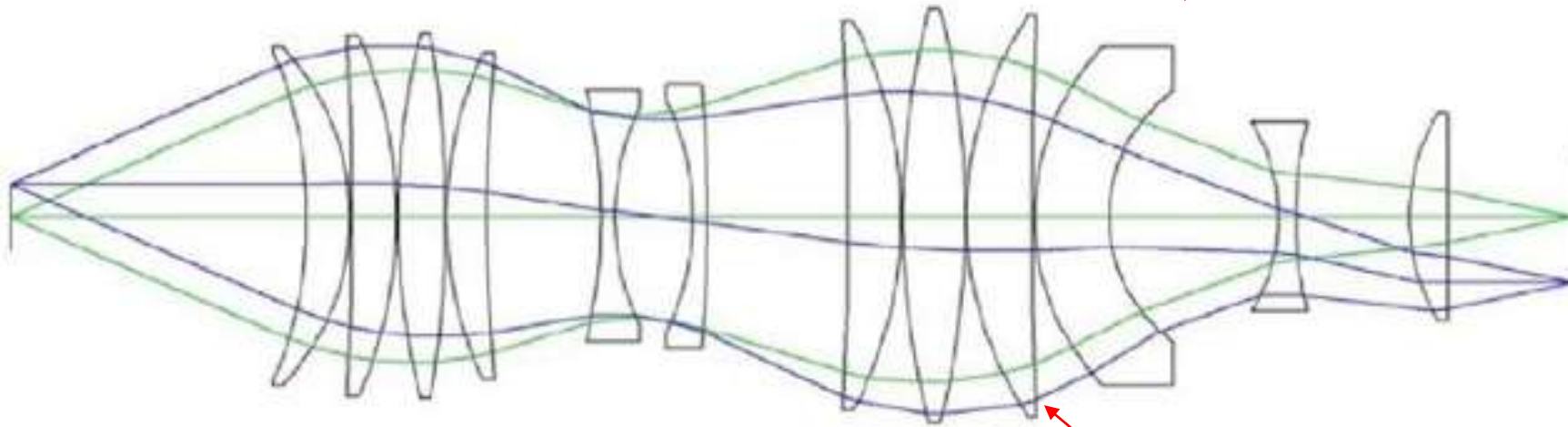
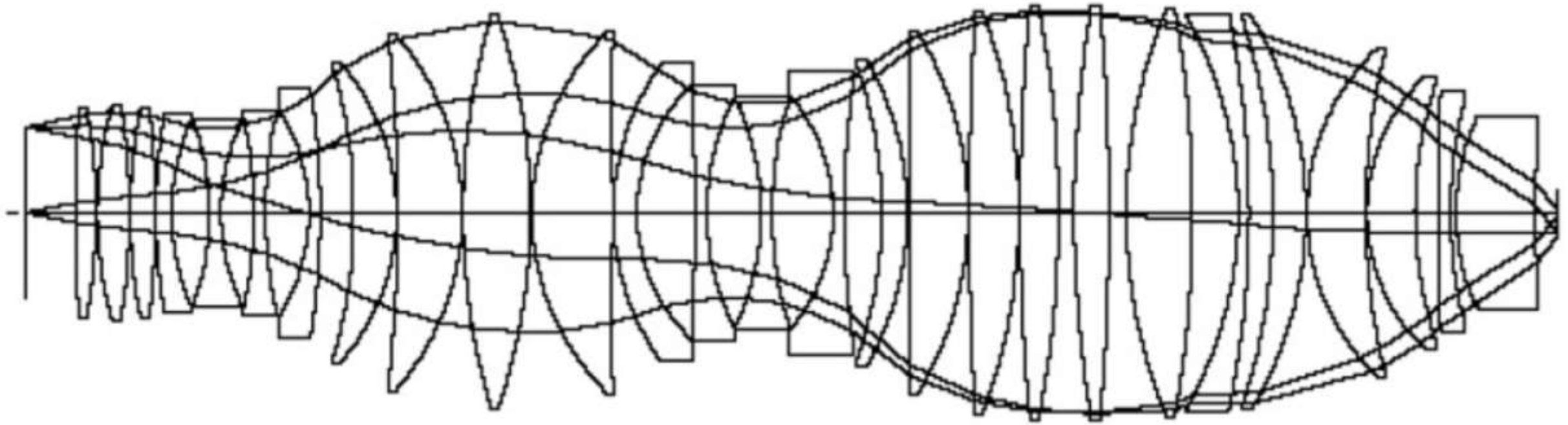


Image quality is. 014 waves r.m.s.
= **3X better than original design**

**Aspheric surface
has been removed**

There is a method for deciding how to replace a lens with one aspheric surface with two equivalent spherical lenses and there is not time here to go into it. The point is that there is such a method and the result here is that aspherics have been used to locate where in the design it is best to add/split a lens to get the most benefit to the design.



This same process of using 3 or 4 aspherics spread out through the length of the design can be used with very complicated designs like this to easily and quickly find out what part of the design would best benefit from an extra lens or two. And it can do that **without** having to first actually do the lens splitting or adding of a lens(s). This use of aspherics during optimization even correctly predicts **beforehand** how much improvement there will be in performance (wavefront correction over the field) **after** all the aspherics have been removed and equivalent extra lens(s) added. Very useful!



My time is up.
Any questions?